

LEVEL

PROPERTY OF THE
FLA. STATE GEOL. SURVEY
NO. 12.

Levels

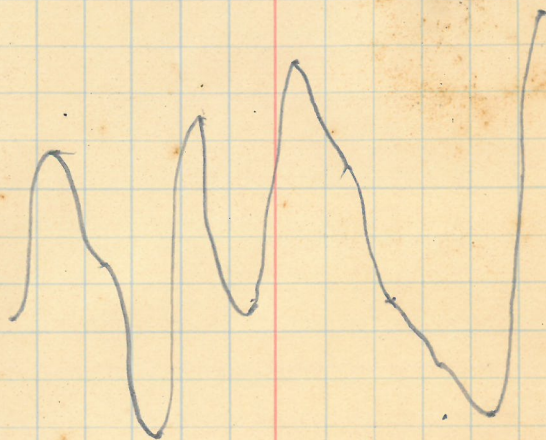
1917

No. 12.

Beards of Tallahassee

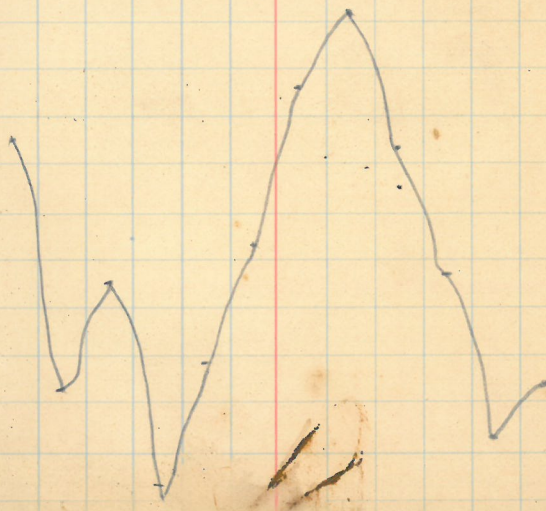
Jan. Feb. m. A. M. 2. 9 A. 8 P. N. L.

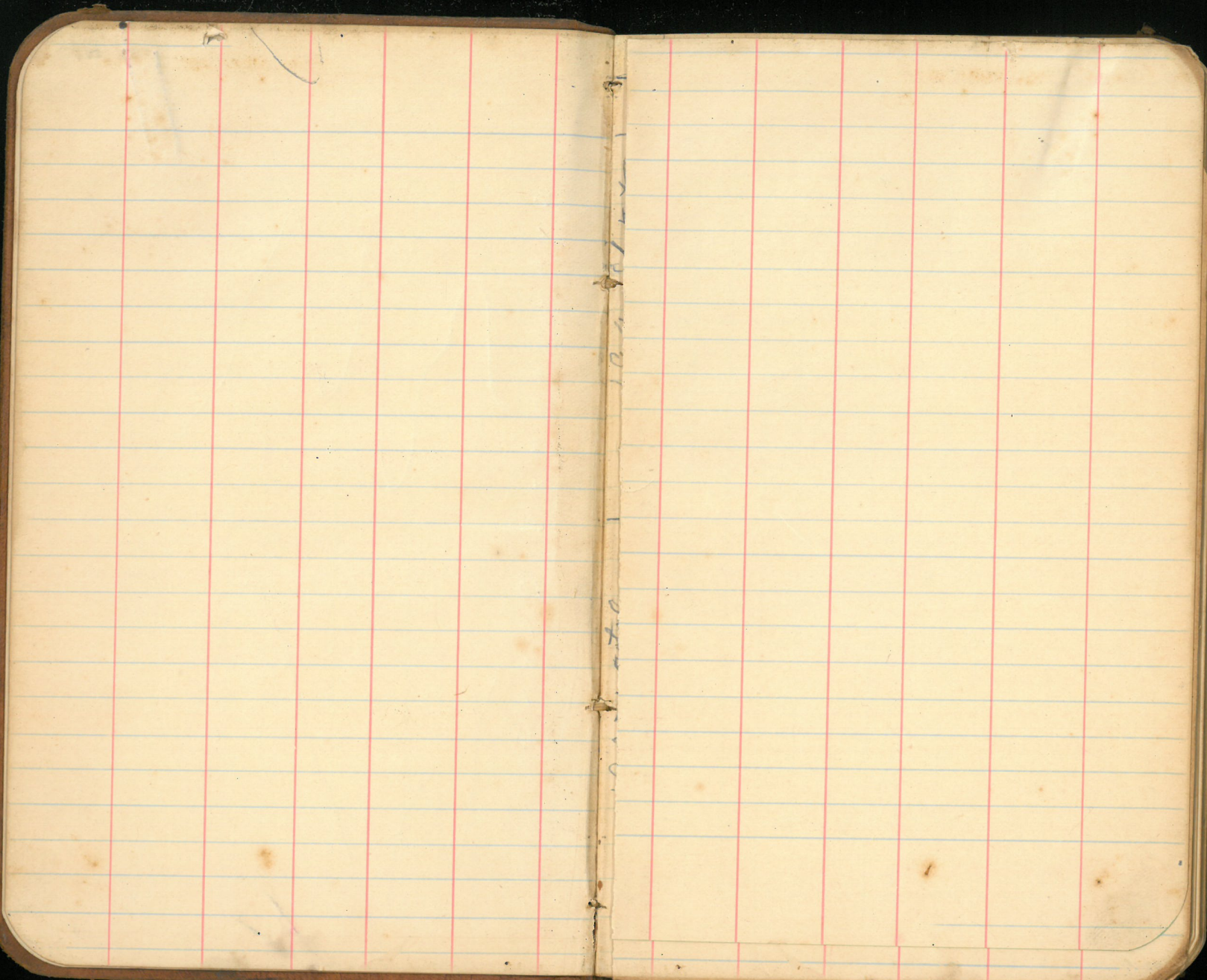
9.
8
7
6
5
4
3
2
1
0



1906

10
9
8
7
6
5
4
3
2
1
0





1907 total
64.79

1908 total
55.

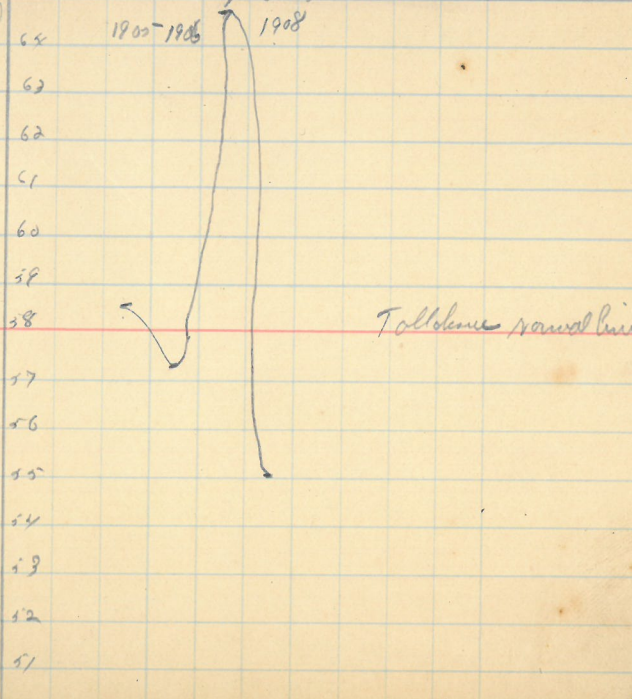
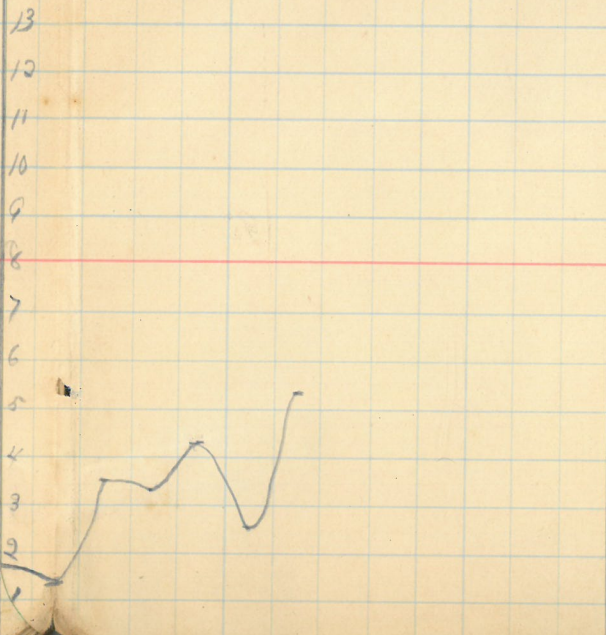
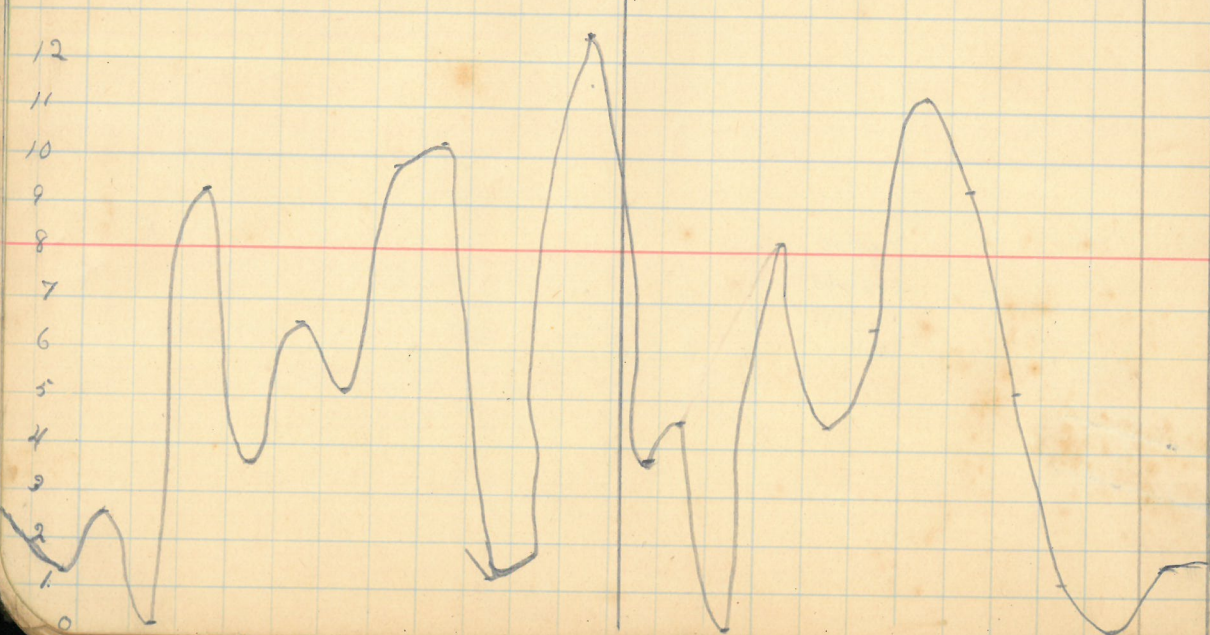
1909

Summary for years 1905-1909.

Jan Feb Mar Apr May June July Aug Sept Oct Nov Dec Jan Feb Mar Apr May June July Aug Sept Oct Nov Dec

Jan Feb Mar Apr May June July Aug Sept Oct Nov Dec

1905-1906 1908



Tollblom's record line

1905 Total 58.53

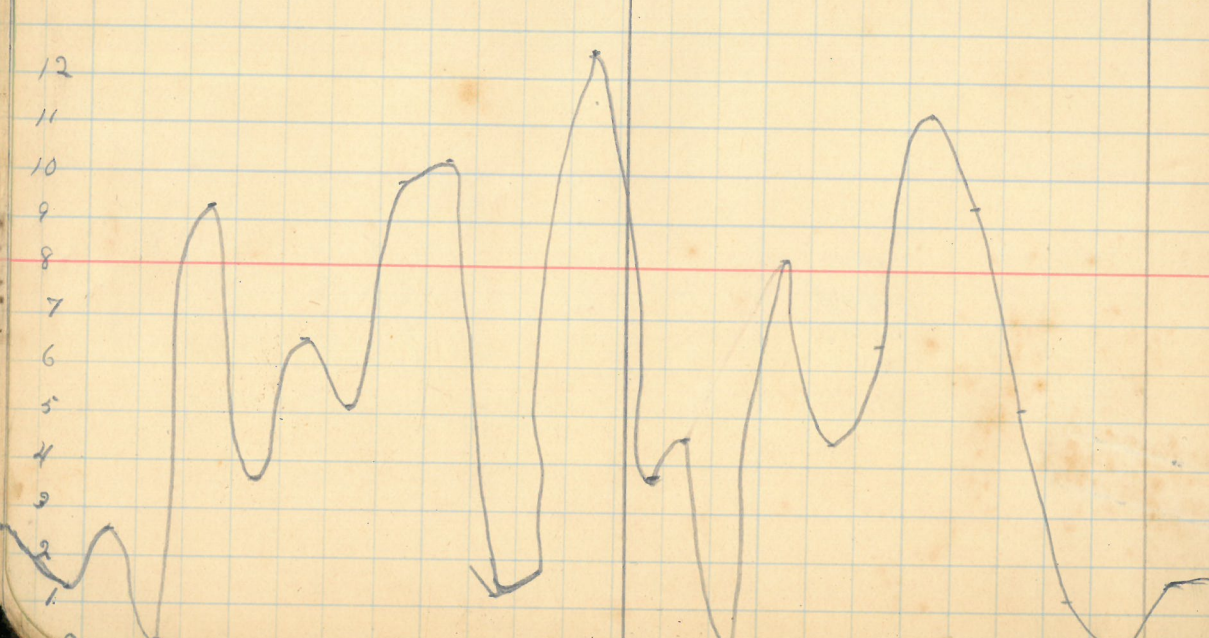
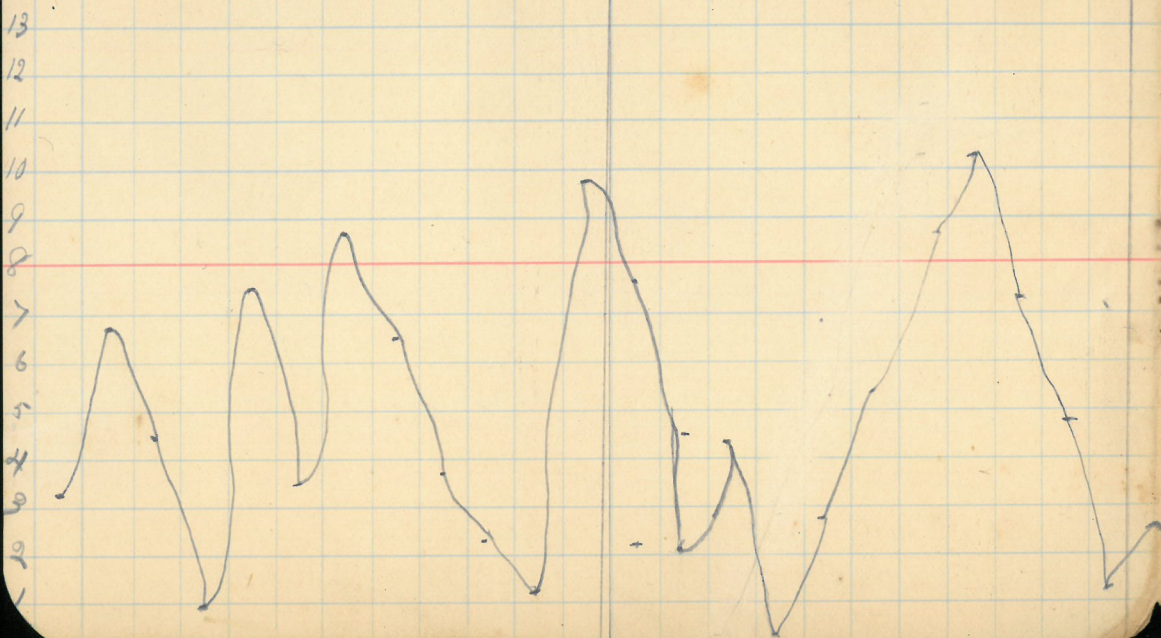
1906 Total 57.20

1907 Total 64.79

1908 Total 55.

Jan Feb M A M J J A S O N D Jan Feb M A M J J A S O N D

Jan Feb M A M J J A S O N D Jan Feb M A M J J A S O N D



Brayford at Tallahassee

Jan. 09 2.97
 Feb. 09 2.96
 March 09 2.97
 April 09 2.96
 May 09 2.97
 June 09 2.97

Sept. 08 2.97
 Oct. 08 2.96
 Nov. 08 2.97
 Dec. 08 2.96
 Jan. 09 2.97
 Feb. 09 2.96
 March 09 2.97
 April 09 2.96
 May 09 2.97
 June 09 2.97

W. H. Northam
 July 5.15
 Aug. 6.03
 Sept. 4.72

88.14 - 18.93

60.89 + 8.68

60.80 + 8.73

60.84 + 2.95

68.95 + 10.81

14.96 - 12.85

60.68 + 5.30

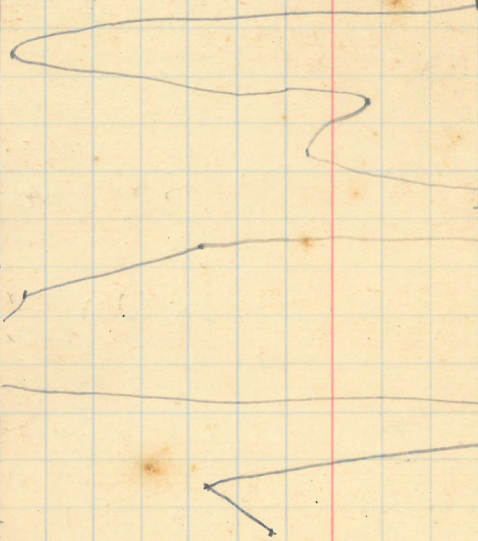
89.33 - 2.6

6.89

6.46

of all months

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64



Normal of
 Tallahassee

58.1

64 63 62 61 60 59 58 57 56 55 54 53 52 51

Samsville June 09 41.98 - 2.68
 May 09 1.53 - 1.34
 Apr 09 1.02 - 1.15
 March 09 1.88 - 1.58
 Feb. 08 1.71 - 1.59
 Jan. 09 3.15 - 0.40

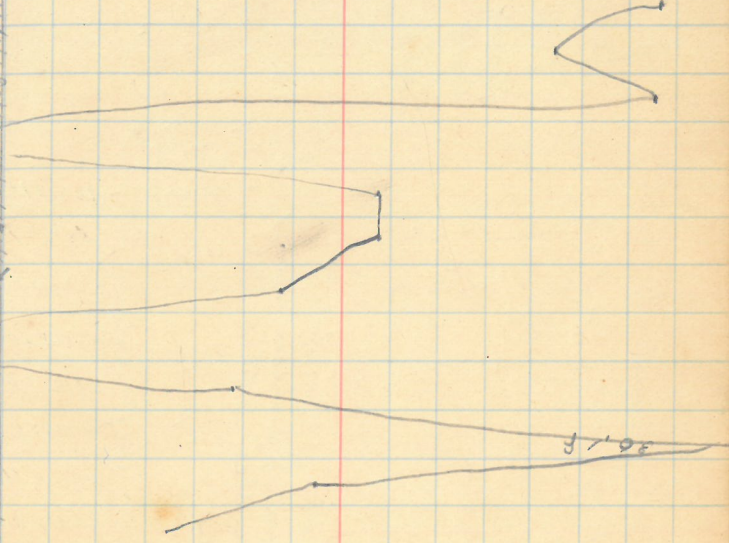
Observer.
 J. P. H. Bell.
 July 16. #1
 Aug. 4. 8 #
 Sept. 1. 2 #

Breeds at L-h City incomplete for 1906 - Rainfall first ten months
 52.42 in. which is above normal for the ten months 8.03 inches.
 Rainfall at Jasper Nov. & Dec. Nov. 1.53, off by 2.2 city inches 52.95 -
 Rainfall at Macleary Nov. & Dec. 1.18 " " " 53.60
 Rainfall at Samsville Nov. & Dec. 1.86 " " " 52.88
 One of these three 29.85 " " " 53.49

59
 58
 57
 56
 55
 54
 53
 52
 51
 50
 49
 48
 47
 46
 45
 44
 43

Samsville

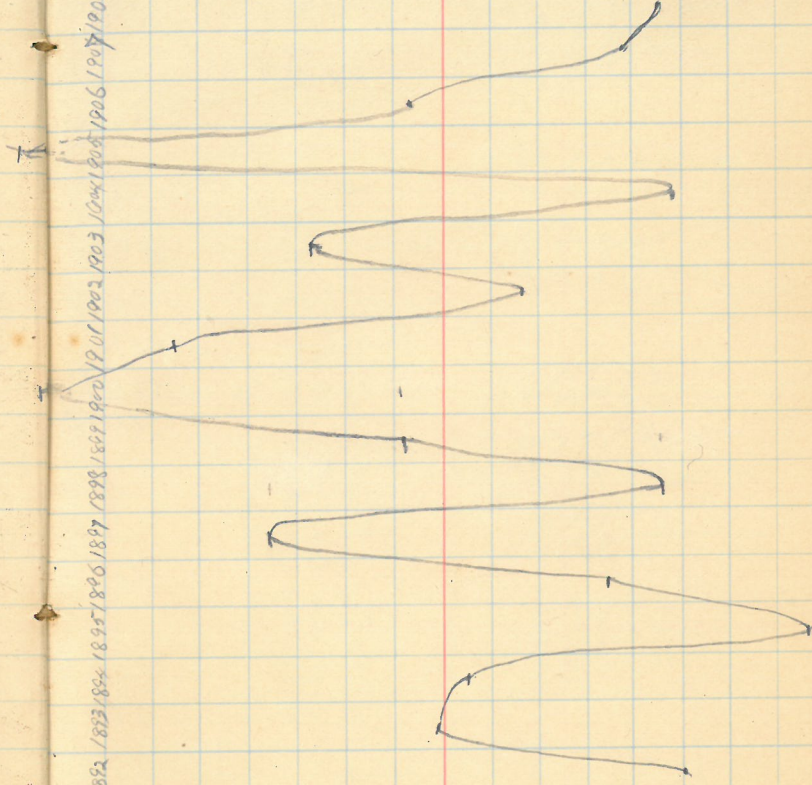
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31



Normal
 Samsville
 50.53

60 1894/189 1882/1883 1884/1895 1886/1887 1888/1889 1890/1891 1900/1901 1902/1903 1904/1905 1906/1907 1908/1909 1910/1911

59
58
57
56
55
54
53
52
51
50
49
48
47
46



Normal
in the
stat 5.2+

Total Deposits

Brookville Jan. 09 - 1.19
 Feb. 09 - 1.62
 March 09 - 1.40
 April 09 - 1.82
 May 09 - 4.79
 June 09 - 6.04
 Observer: C. C. Peck
 July 18.88
 Aug 8.95
 Sept 2.09

See note on Brookville over.

Receipts for 1907 at Brookville deficient. March + April lacking.

Rainfall for ten months 43.80
 at st. des. March and April. 1.66
 at Governor " " 1.53
 " " " 1.54

64
63
62
61
60
59
58
57
56
55
54
53
52
51
50

29.87
67.86
64.34

52.27

53.27

31.64

59.79

61.01 + 3.22

18.65 + 2.04

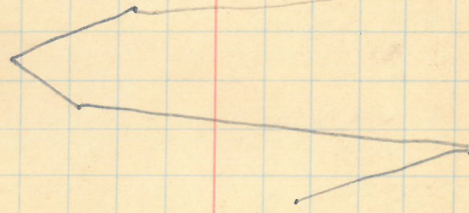
45.04

53.40

17.14 - 10.18

1894 18.82 18.93 18.94 18.95 18.96 18.97 18.98 18.99 19.00 19.01 19.02 19.03 19.04 19.05 19.06 19.07 19.08 19.09 19.10 19.11

64
63
62
61
60
59
58
57
56
55
54
53
52
51
50



Only 3 months recorded.

45.94

45.98

45.94

Normal at Brookville 56.80 ±

Moriana Lon. 09

Feb. 09

March. 09

April 09

May 09

June 09

Tidal

0.47

3.08

3.56

4.58

2.52

3.90

Latitude

-3.35

-2.10

-1.93

+2.42

-2.62

-0.34

Observer

R. S. Behrman

Moriana

Brookville cont. - Record incomplete for 1902, March + April lacking.

Rainfall for ten months more. 41.04.

Rainfall for March + April or 84 dec. 3.52

" " " at Lawrence 6.28

One

$$\begin{array}{r} 2 \overline{) 19.81} \\ 4.90 \end{array}$$

$$\text{At Fly Brookville} = 45.94$$

Brookville cont. Record for 1903 incomplete. lacking April to Sept.

Record for five months gone & Feb. + Oct. & Nov.

Record at 84 dec for summer months.

" " " " "

$$\begin{array}{r} 20.65 \\ 37.05 \end{array}$$

$$14.55$$

$$38.85$$

$$53.40$$

$$\begin{array}{r} 2 \overline{) 77.70} \\ 38.85 \end{array}$$

Lainaville Record for 1897 Lechberg made

Rainfall for 11 months

" at Arch for month 0.83

" " Lake City " 2.89

213.72
1.86

34.32
1.86
36.18

Lainaville 1897 Very deficient, mostly for 11 months

Rainfall for 11 months 22.54

at Arch for 11 months 8.18

Lake City " -

14.06
222.24
11.12

42.54
11.12
53.66

Records from 1891

Archer
 Brookville
 Eamsville
 Lake City
 Tallahassee

Sept. 5.62
 Oct. .47
 Nov. 1.80
 Dec. 2.84

0.95 1.00 2.96 3.00

1892

	Jan	Feb.	Mar.	Apr.	May	June	July	Aug	Sept.	Oct.	Nov.	Dec.
Archer	2.57	.32	1.38									
Machine		2.26					20.19	4.85	1.15			
Tallahassee	6.35	2.58	1.40	.85	1.63	8.76	7.68	6.43	3.00	(1)	(2)	6.89

(1) Not needed, one for set above named. (2) Not needed

Archer 1893. only 6 new wells

80.98

Arch 1894
1895-

1895-

✓
Acker 1896 36.2d.

	Jan	Feb	Mar.	1895	June	July	Aug	Sept.	Comp. Nov. Dec.
Arden	2.05	3.34	3.33	4.48	3.77	9.84	5.08	2.36	1.02 4.00 1.78
Bamb.	4.37	4.86	1.98		5.44	12.23	9.84	4.85	1.93 2.23 0.89
L. Cit	5.86	4.02	3.59	4.27	5.03	9.13	5.11	1.14	4.02 2.76 1.58
Talla	6.80	3.22	6.83	3.35	3.95	8.27	9.90	4.31	1.96 2.21 2.34

	Jaw	F-6	Mor.	895	May	June	July	Aug	Seth.	Cash	Nov.	Dec.
Aralen	25.05	3.34	9.33	1898	5.24	2.77	9.84	5.08	4.36	1024.00	1.78	
Bombv.	4.37	4.86	1.98		6.97	5.44	12.23	9.84	4.85-	1932.23	0.89	
L. Cit	5.86	4.02	3.59	4,27	2.56	5.03	9.13	5.11	1.14	1402.76	1.58	
Talla	6.80	3.22	6.83	3.35	3.68	3.95	8.27	9.90	4.31	1962.21	2.34	

Location	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100	2101	2102	2103	2104	2105	2106	2107	2108	2109	2110	2111	2112	2113	2114	2115	2116	2117	2118	2119	2120	2121	2122	2123	2124	2125	2126	2127	2128	2129	2130	2131	2132	2133	2134	2135	2136	2137	2138	2139	2140	2141	2142	2143	2144	2145	2146	2147	2148	2149	2150	2151	2152	2153	2154	2155	2156	2157	2158	2159	2160	2161	2162	2163	2164	2165	2166	2167	2168	2169	2170	2171	2172	2173	2174	2175	2176	2177	2178	2179	2180	2181	2182	2183	2184	2185	2186	2187	2188	2189	2190	2191	2192	2193	2194	2195	2196	2197	2198	2199	2200	2201	2202	2203	2204	2205	2206	2207	2208	2209	2210	2211	2212	2213	2214	2215	2216	2217	2218	2219	2220	2221	2222	2223	2224	2225	2226	2227	2228	2229	2230	2231	2232	2233	2234	2235	2236	2237	2238	2239	2240	2241	2242	2243	2244	2245	2246	2247	2248	2249	2250	2251	2252	2253	2254	2255	2256	2257	2258	2259	2260	2261	2262	2263	2264	2265	2266	2267	2268	2269	2270	2271	2272	2273	2274	2275	2276	2277	2278	2279	2280	2281	2282	2283	2284	2285	2286	2287	2288	2289	2290	2291	2292	2293	2294	2295	2296	2297	2298	2299	2300	2301	2302	2303	2304	2305	2306	2307	2308	2309	2310	2311	2312	2313	2314	2315	2316	2317	2318	2319	2320	2321	2322	2323	2324	2325	2326	2327	2328	2329	2330	2331	2332	2333	2334	2335	2336	2337	2338	2339	2340	2341	2342	2343	2344	2345	2346	2347	2348	2349	2350	2351	2352	2353	2354	2355	2356	2357	2358	2359	2360	2361	2362	2363	2364	2365	2366	2367	2368	2369	2370	2371	2372	2373	2374	2375	2376	2377	2378	2379	2380	2381	2382	2383	2384	2385	2386	2387	2388	2389	2390	2391	2392	2393</
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City	5-59	4-27	2-56	3-03	9-13	5-11	1-14	402.76	1-58
L. City	5.86	4.08	3.59	4.27	2.56	3-03	9-13	5-11	1-14
Tulla	6.80	3.22	6.83	3.35	3.68	3-95	8.27	9.90	4.31

[illegible]

1896

Fall

2. 0. N we

9.608.60 s. 12. 18

machu

Tallabone 1896 11 min Pond sample 64.

Tallabone 1886. 66.66; 1887 58.75; 1888. 68.49;
monitors 1891. 1889 48.84; 1890 53.57
1891. 44.85-

1,94 3.55 5.51 2.93 6.61 2.84 4.47 8.43 4.67
1.30 1.28 2.93

monitors 1902 Total 37.75-

Talla 1892 (Nov. Looking S)

93 60.96

94 52.88

95 50.01

96. Just looking.

Garneswell 1891

May 3.09 June 8.89 July 4.23, Aug 9.27 Sept. 3.91

Oct, 4.4. Nov 2.62. Return being

Inclosed to line June 18/915

This elev. is a check on

Pool ^{at} South side of Lake John^o
Aug 23 5.6 8.5 - 2.7 = 6.80 ft 4.4 =
5.1

8.15

former reading of height from bench to
between Mables & Lake John Station

$$55 - 5.6 = 29.4$$

$$50 - \frac{5.1}{2.43} = 25.7 \text{ elev. of divert.}$$

$$10.6 - 5.6 = 5.0 \quad 2.45$$

5.6

Red

cluster

angle

$$7.1 \quad 8.9 - 5.4 = 3.50$$

0

$$9.3 \quad 11.45 - 7.25 = 4.20$$

$4^{\circ}15'$

$$9.1 - 7.1 = 2.4$$

sta

Bs

Fs

H. 2

Lake

7.1

7/

Sta

BS

FS

#9

Elev.

7.1

7.1

7.1

Series at the north end

Sta. B.S. F.S. H₂ Rod Elev.
Bm 0

140 7.1 7.1 2.85 4.35

280 13.65 18.00 2.85

320 6.125 3.6

270 9.00 6.0

275 4.35 76.65

320 8.6 100.8

200 4.50 101.5

270 6.25 71.6

50.35 48.8

of Orchard pond aug. 23 1917.

Lake Level.

5.65 - (at 140, angle 1°10') 2.80 = 2.85

7.25 + (dist 280 angle 1°20') = 6.40 = 13.65
6.25 dist 7.7 - 4.5 = 320 ang 4.20 = $\frac{24.00}{6.1}$
18

10.5 - 7.82 = 270 angle 3°15' = $\frac{15}{24}$

5.7 - 2.95 = 275 44°20' = $\frac{21.4}{435}$

10.2 - 7 = 320 2°50' = $\frac{15.65}{15.5}$
8.6
24.1

8.5 - 3.5 = 200 1.45 6

76 - 4.9 = 270 5° 1.5

7.6 - 4.9 = 270 5° 2.2

10.2 6.25 22.25

11.65 - 9.2 = 245 3° 12.5

103

228

Levels on the east +

From Stake #2 level 48 ft

1 st	H.S. 10.2	12 - 8.4 = 360	2.50
	F.S. 3.1		20 0
2 nd	7.9	10.8 - 5.0 = 580	1.50
	F.S. 7.5	10.12 - 4.2 = 595	1.40
3 rd	9.2	11.9 - 6.5 = 540	1.10
	F.S. Transfer of line to top of		
	L.S. " "	to " "	
	F.S. " "	" "	
4 th	10.65	12 - 9.3 = 270	1.10
5 th	7.25	9.45 - 5.15 = 430	3.10
	F.S. 10.45	11.4 - 9.55 = 185	2.05

From B.W. 101/2 center

1 st	9.6	11.75 - 7.50 = 425	2.40
	F.S. 10.18	12 - 8.3 = 370	3.15
	H.S. 10.5	11.7 - 8.45 = 325	1.25

To line to Red house on hill across to
club and back shows the 1st line
for center.

North-east side of Circle post - aug 1877

above Circle post

			level of post, above White
		$= 18.11 + 10.2 = 28.31$	48 = 76
		$= 19.61 + 7.9 = 27.51$	88.8
		$= 17.61 + 7.5 = 25.11$	75.3
		$= 11.51 + 9.2 = 20.71$	75.3
		$= 20.71 + 7.3 = 28.01$	
		chimney of small house $\frac{1}{2}$ mi. North, Boker's	
		roof " " yellow, across to Lake 20° W & N.	
		Twice length of chimney, of house 20° W & North.	
		40 ft up in about 10 ft above last a 106.0	
		$= 5.5 + 10.6 = 16.1 + 10.6 = 26.7$	level 79.3
		$= 23.60 - 7.25 = 16.35$	$79.3 - 16.35 = 21.63.0$
		$= 6.7 + 10.45 = 17.1$	$63 - 17 = 46 ft$

		$= 19 ft$	$101 - 19 = 82$ level of east
		$= 21.1 + 10.1 = 31.1$	$82 - 31.1 = 51$ level
		$= 8 ft$	$10.5 - 8.4 = 16 = 51 - 1.4 = 50.2$
		then which is $82 - 10 = 72$ + corner	
		of Houseman's house stake between the 50 + 75	

Level: trees from base of House
to South side river are level
about 5 ft higher or about 72 ft.

Levels at Crossing of S.F.A.

Aug 24 Okla. River level = 0

Top of rail on bridge = 22 ft.

1st Int. H² 10 ft

2nd B. 12.0

2nd Int. 9.1

F.S. 1.7

Insert tab of instrument for

3rd Int. 4.55 1-5 600 ft.

Distance out for 60

$$72 \times 3 = 216 \text{ ft.}$$

$$161 \times 3 = 483$$

on Oklahoma River.

Level of river $22 + 10 = 32$ ft. Level of 2nd
= 32... " " bank

" " $32 + 9.1 = 41.1$ " Int

" 1st Bank = $41.1 - 1.7 = 39.5$

at 60 1/2 mi is $41.1 - 1.25 = 39.85$ ft.

$39.85 + 4.5 = 44.35$. Level 2nd of cor

Probably 10 ft above level of 60 ft.

$\therefore$ Level of water in River about 75.45

Levels to tie up St Augustine Road,

H.O. H. 2 F.S. Elev

T.P. 2/4.9 1.1 = 23.881

F.S.

T.P. 2 128.051

10.38

203.457

6.0

181.757

Level transferred to St Augustine Rd

T.P. 2.25 144.50

3.80

108.70

T.P. 1.00 110.701

4.05

126.157

Assumed elevation 182. actual 126.157

Hill at S.E. camp Smith points

Malloy hill lower by about 10

Red tile roof in magnolia Heights

Hills north of Lake Lafayette

hills 1045 high on 215.

Station 103. No elevation given.

100 ft = 155.84

75" = 130.8

50 = 105.8

25 = 80.8

200 = 255.8

175 = 230.8

150 = 205.8

125 = 180.8

100 = 155.8

75 = 130.8

50 = 105.8

Bench on capital 214.931

angle

2.7.2 - 1.26 = 146 ft

2° 58' = 7.8

7.25 - 4.8 = 245 ft

2° 24' = 10.3

Starts about 1 ft below sleeping porch screen

4.30 - .20 = 410 ft

5° 35' = 38.5

5.76 - 1.76 = 400 ft

4° 31' = 37.95

7.25 - .80 = 645

1° 45' = 19.5

Assumed 55.843 too high.

Probably misstate 66. 215 ft.

or 15 ft

Level with corner. nearly same height.

Seems to be more than the height of on slope

4 m just as about 206 or 207

Elevation from West Rail of

Line of Jefferson to here

Bench H.S. L.S. F.S. Elev. 124.41

2.45 126.86

4.5 122.36

4.45 116.75

9.45 106.70

Flow of bridge & General level
Level of limestone into which
5.6

6.35

0

8.7 106.78
15.105 10.45
5.6 94.35
9.45

Level of course of stream bed at
Transfer of level from Hill of
Hill on north side of Lake
trees. White house among trees

Low level on Capitol's road too high by about

Low line S.A. Rail at Chain

A.C. & Phenix of Crest Line & Stearns of
creek

Bench of Road left. West end of trail of course

4.25 - .65 360 ft. direction of road

6.5 - 2.5 = 400 " 38° East of south,

7 - - 2 = 500 " angle 10 14'

11.45 - 7.45 Low Flood bridge

about 3 ft. to water level 6 ft.

But Bush brush rocks.

Level of top of limestone

97.34
55.84

41.50

this course about 48' ft. Low water 44'

4 m put on 88 opposite. Road old 116 ft

seems to be lower by more than the height of the

low by fully the height of the large trees 40' 30'

East of N.

200.3 106.3 200
106.3 55.8 13.2
95.5 53.5 146.5 ft.

200.3
146.3
53.8

Arthur Robinson's place, on chain
 just $\frac{1}{2}$ m from town on line with
 Henderson's farm. Also level of
 Mason Hill. Somewhat above
 Maloy Hill. Level of St. Augustine
 road.

Level to connect Jones levels at Chaires.

Bm H.S. H.P. F.S.

3.425 63.640

4.600

5.975 65.015 7.150

Chs 215-

58.040

57.865

M.S. Corp Survey 246 west 50 feet of Chaires

Jones level was $\frac{200.3}{58.04}$ Jones to high by
 $\frac{141.26}{199.15}$
 $\frac{57.86}{141.31}$

Connection of Jones levels with
 Jones bench around 200 was
 necessary line of 530 + 531

Difference $\frac{200}{115.21}$ line of error at 1 ft.
 $\frac{84.59}{}$

Jones level 200 = $\frac{200}{141.3}$ at level
 $\frac{58.7}{}$

There of McCarrie Co on St. Augustine road,
 on a stump probably about 1 ft high.
 = 114.41. Travers to stump level (at 115.21)

Levels of Lake Lafayette Elev.

#9 F.S.
H.S. 4.1 53.10
10.4

Base Bench mark of M.P. 158 49.00

$$10.75 - 10.05 = 70^\circ \text{ angle } 10^\circ 35' = \frac{10.4}{1.8}$$

$$\frac{53.10}{12.3} = \text{Elev. Gen Lake basin } 40.8 \quad \frac{12.3}{40.80}$$

H.S. 4.1 53.10 2.3 50.70

6.6 57.30 10.85 46.45 =

0 46.45 7.8 38.65 =

5 43.65 = Level near mid height of groups of posts in sink N.W.

also near the top of the posts of the fence at gate south of the house near the sink.

The level 46.45 transferred to the sink = level on large oak tree south of the house about 2 ft from base and 2 or 3 ft over top of posts of fence

Level on Thomasville Road
Station 0 on oak tree (top of Bench)

H.S. L.S. F.S. Elev.

actual Level on Thomasville Road
as figured from the assumed level

1. Maximum of hill at Beard Place is → Station 4 $205.8 + 12.36 = 218.16$ ft
 2. Lowest level in depression beyond entrance to Winthrop place Station 91 = 98.16 "
 3. Top of hill. Station 131 $193.3 + 12.36 = 205.66$ "
 4. Top of hill at station 188 (3 1/2 mi from city limits) $209.7 + 12.36 = 222.06$ "
 5. Long level plateau miles Johnston & beyond is between 200 & 215 ft.
 6. Top of hill at station 325 (6 mi) $204.1 + 12.36 = 216.46$ "
 7. Public road at entrance to Lake Hall Station
 8. Lowest level in depression at Station 362 (6.8 mi) $80.9 + 12.36 = 93.26$ "
 9. Top of hill, station 457 (8.6 mi) from city limits $212.5 + 12.36 = 224.86$ "
 10. " of " " 480 (9 mi) " " " $226.11 + 12.36 = 238.47$ ft
 11. Lowest level in long depression at station 728 (13.7 mi) $96.32 + 12.36 = 108.68$ ft
 12. " " " depression at station 818 (" mi) $91.3 + 12.36 = 103.66$ "
 13. Elevation at Bench of state line? Station 957 + 43 ft (18.1 mi) = 1000.08 "
- All the land is of only moderate height from the high hill at station 480 (9 mi) to the state line.
14. Gomonie Slough station no 821 is $90.7 + 12.36 = 103.06$

Rail County Engineer.

25' RL of 200 elevation. Elev. on road 200.
Bench. S.E. corner State Sec. 38. 216.040
actual level of Bench on Thomasville
Road is 212.36 ft

Assumed level is 12.36 ft over low.

actual elev.

See these levels as checked Sept. 14 1917

Levels on Bainbridge Road

Level on Bridge 50' back from 1st bend

H.S.	L.S.	F.S.	Elev.
3.45	203.45	5.75	197.70
5.05	202.25	4.70	198.05
11.40		.95	208.50
9.65		.70	217.45
2.05		9.50	209.90
9.85		.25	219.50
11.00		4.00	226.50
11.70		1.00	237.20
11.60		.45	248.35
11.25		.50	259.10
11.60		1.35	270.35
9.60		3.95	276.10
6.65		10.30	272.35
3.25		6.50	269.20
.4		3.75	
12.30		.55	
8.85		.65	
11.50		2.05	295.25

2000 level on road at 200 is 116.66
or 83.34 too high.

Jones. B.M. on iron cor. city limits
(on right of road?) assumed. Elev. 200.

Floor of Bridge on Chickasaw River 183.

Station 305 (Lake Jackson) 180.7

Levels on the Bainbridge road are

83.34 feet too high

Floor of bridge at Chickasaw is

183 - 96.89 =

86.11 ft

When rechecked Sept 14 1917.
Jones Levels found to be 88.35 too high
∴ apply correction accordingly.

Top of curb at intersection of N. Monroe and North
Line street or Quincy Road. Actual Elev. 192.76

End of curb on East side of Calhoun St. at
intersection of North Line St. Act. elev. 185.86

Back zero on Thomasville Road, oak tree, top of
right Bank at City Limits. Act. elev. 211.91

from corner on Calhoun St

HS

11:05

7:20

2:70

4:50

11:70

8.275

FS

.70

3.80

8.15

3.95

(NS) $6\frac{1}{2} - 4\frac{1}{2} = 140'$ angle $3^{\circ}57'' = 9.6 + .5 = 10.1$ up.

.5"

.86 below bench

299.38 -

Coast + Geodetic Survey bench mark on
State Savings Bank. Act. elevation 216.04
i.e. Jones' levels are 83.34 too high

On Bamhedge Pond

See current level following.

General levels, Dornhede road.

1. Lowest depression in city limits on
2. Top of hill, station 49 (uni obs)
3. Continued high elevation
4. Lowest depression at station
5. Top of hill about 4 mi out
6. Lowest depression near lake
7. Level of Lake Jackson Basin
8. Level floor of bridge of Akkabeu
9. Water level in Akkabeu
10. Station 340 + 70' Lake Jackson
11. Depression west of Michels Sta
Water level in Lake Jackson

		actual El.
this road	$197.70 - 83.34 =$	114.36
from at least 3 1/4 mi	$1 - 83.34 =$	230.76
max. at Sta. 91, 324.5	$- 83.3 =$	241.10
130 is	$228.77 - 83.34 =$	145.43
Station 165 is	$331.3 - 83.34 =$	247.96
Jackson Sta. 305 is	$180.7 - 83.34 =$	97.36
below road is about 25 ft		
is	$183 - 83.34 =$	99.66
possibly about	$98.60 - 22 =$	76.60
Sta. 211.94	$- 83.34 =$	128.60
319	$197.6 - 83.34 =$	114.26
Basin.	$114.26 - 25 =$	89.26

Note all these levels circled by adding 7
5.01 ft.

General for St Augustine Time Road

Deposits at Stations 316 is

Pond just east of road is

Levels St Augustine Road to

Beach on St Augustine Road

530 of St Augustine road

530 of " " "

530 of " " "

Sta Elev. Dist.

48 187.5

138+10 187.9

190.4 Top of stream bank

192.4 Floor of bridge

158+5 200.4 Top of S a L. 100'

160 199.1 Land level at Capitol

182 204.4

206 196.4 swamp

267 215.8

295 195.2 Bottom of creek

334 223.3 High land near Co line

339 218.0 County line

217.2 - S a L top to of

Time Road

133.8 (actual 77)

about 8.7 lower 7 less 67 ft actual.

Chairs Station Capitol & Co. line.

Coast Swamp R 75' owned road actual 58.7

on this bench is 197.9 56.6

on profile is 109.2 43.5

" Road level is 108.3 53.5

46.2

46.6

49.1

51.1

went 7 dist.

59.1

57.7

63.1

55.1

74.5

54.6

82.0

76.7

County line

75.9

Levels in Jefferson County				
Bm	H.S.	L.S.	F.S.	Elev.
	5.975		8.7	
	3.750		5.6	
	5.725		4.35	76.925
15.450			4.925	77.285
			3.025	77.385
			4.80	77.160
			10.00	71.475

Channel of stream under iron bridge

Bench at east side of 1st bridge north
assumed level is 98.4 ft too high

Supplied by Mr. Jones

N.S.C. & Ind. Surv. Logs 80.825

1st board at west end of 1st bridge

Last board on East side of 1st " North end

1st board on second bridge North end,

Last board on bridge North end of board.

Average Level of Swampy land

overage about 11 ft. below floor of bridge.

end by Mr. Jones was

$$\begin{array}{r} 175.7 \\ 77.3 \\ \hline 98.4 \end{array}$$

1. Jefferson Co. line
2. Station 43 depression
- " 65 Hill
- " 86 depression
- " 197 Hill
- " 232
- " 286
- 350 Hill
- 376
- 388
- 368+50

549

670 in front of Ford

Top of Rail S. side at chert across
Bottom step south side of Courthouse

Land in Swamp E. of Logh

Sage

200 ft N. of depot
at Monticello

annul.	actual
200	101.6
173	74.6
187.5	89.1
172.	73.6
222	193.6
250.5	152.1
232.	133.6
300	201.6
225	126.6
308	210.6
311.00	212.6
182.	93.6
337	238.6
310.00	211.6
335.79	232.35

Lixie Highway east. Station

167 Floor of bridge on Wolf
178
281

Bm Tel R of Tumbul

Thomasville Road.

Court House Steps B.M.

Some bore es line from

B.M. nail in tel. pole on

59. A.C.L. Crossing

199 Depression water level

290 " water "

397+65 Creek water level

Fill of Creek Bottom of

402 on pine stump & left

268 Hill High point on road

State line probably

(Bm west from Northville)

6702 = 0 New assumed bore 200

Creek Bridge

197.80

238.

214.

Stone Nail.

South Side bottom step. 335.79

Jefferson to line.

R. of Station ~~xx~~. assumed at 200.

actual is 222.12

136.1 actual.

158.22

85.00 107.12

78. 95.12

71.9 94.02

74.5 96.62

76.05 98.17

154.00 176.12

Gully Branch.

Floor of bridge

+ 40'

about

100 ± 122.12

Six to Highway Aucilla west.

0. Aucilla River Floor of Bridge
Station Wakulla

Capps

Boyer Hill

Climb 2 mi from River

Depression about 3 mi

about $1\frac{1}{2}$ mi.

Hill $2\frac{1}{4}$ mi west of River

about $1\frac{1}{2}$ west of $2\frac{1}{4}$

195

275

302

Six mi from River

$6\frac{1}{2}$ mi from River

413

8 mi Capps

464

9 mi from River

530

640

Cherry tree corner.

654470 Bm on Oak tree

Assumed

200

253

316

276

212

206.

280.7

212.

267.9

288.

344

338.

282

339

324

on left at Cross Rd 338.30

Sept 6. Levels at Monticello ^{Actual}

H.S. L.S. F.S. Elev.

4.8 9.7

.1 11.0

.0 .1

10.65 194.63 .3 194.43

4.20 218.13

.3 217.83

2.3 220.13 4.9 215.23 @ 37.35

1. Mr. Jones assumed bench on

A.C. Left of S.A.L. left

H.S.

F.S.

7.5

6.85

Ticks office S.A.L. Top of rail

" " A.C.L. " "

Mr. W. Jones, County Engineer, Jefferson Co.

Jones Thomaston River. Bench assumed 200
Bench on Tel. pole 2nd South of fork of Road

$$7.5 - 8.5 = 66.5 \text{ ft angle } 1041' = \frac{19.5}{4.2} = 23.5$$

Top of bottom step of Court House

at the South side

Thomaston river is low by 22.2 ft.

Bench assumed 200 = 222.2 actual.

Elev. S.A.L. Top rail 200 ft N. 7 left.

at Ticks office 7.25 S.A.L.

of 2nd track

1st track at T

actual

212.0

212.2

Sept 6. Levels at Sink near Lays

H.S.	L.S.	F.S.	Elev.
5.0	82.16	4.85	77.3
3.2	74.11	5.70	68.41
9.65	78.65	3.55	75.10
10.9	86.41	9.90	76.50
9.65	86.16	3.20	82.96
5.0	87.96	10.95	77.01
1.00	78.01	6.9	71.11
5.40	76.51	4.1	72.41
9.65	81.06	4.65	76.41
6.30	82.71	2.15	80.56
3.45	84.01	10.3	73.71
4.05	77.76	10.7	67.06
3.35	70.41	5.4	65.01
5.55	70.56	2.35	68.21
4.35	72.56	4.90	67.66
2.20	69.80	3.40	66.46
7.08	59.38	10.1	59.38
	59.38	23.36	36.02
		13.08	46.30
21.42	67.72	4.55	63.17

By L. of
Depression
83 L. 8
Elevation

Pool

Bench last found north end wooden
bridge east side 77.16

East side of iron bridge last found 4 south

Water level in pond to the R. (Elev. 73.5)

Second Small run

at top of Sink West of road. Water in Sink 73.71
40.30
33.20

Bomb of Stream. Top of limestone

Top of bank at Sink of stream

Reading by angle 10 ft - 2.92 = 7.08

Reading F.S. by angle 8.36 + 15 = 23.36' } note

water level in the Sink.

Top of bomb on West side of sink

The valley of this width is about 300 ft.

West of which the land rises gradually.

Levels of Sink with 1 Flych

Sept 6

measure of Sink or left of road

near sink of stream

Base H.S. +L -L

4.85

7.5

7.825

measure top of limestone Elev.

H.S. L.S.

3.35 70.41

7.50

52.91

Failed to read angle reading.
(This level is estimate of H.S.)

Level across Sink

H.S.

2.92

8.36

3.6.02'

2.92

59.38

1.48

2.58

4.55

73.71 Eased level near wall of top of Sink

8.4 - 7.15 angle $180^{\circ} 25' = 177.5^{\circ}$

45.92

4.85

40.45

Base Bank nearby 67.06

9.05 - 8.45 = 60 ft angle about $8^{\circ} 10' = 7^{\circ} 17'$

water level 52 + 6 ft. = 46 ft.

Base top of fault 66.46

3.13 - 2.74 = .39 angle $15^{\circ} 48'$

8.74 - 7.96 = .78 angle $13^{\circ} 8'$

these two readings give water level

3.13 - 2.74 = .39 L $15^{\circ} 48'$

2.04 - .92 = 1.12 ft L $6^{\circ} 00' = 1.48$

13.08

3.15 - 1.98 = 1.17 L $10^{\circ} 50' = 2.35$

21.42

Level of Valley wall of stream, Aug 30

Levels of sink north of Lloyds
7th map.

Level Ind. Last Set up. Elev.

67.72 F.S. 10.55

45.62

7.37

44.12

Stem c. 5 ft old in 100 ft.

11. - 10.1 = 90 ft $\angle$ 70 15'

Level of stem a 80 ft from Ind.
720 West of south

8.12 - 6.7 = 132 ft $\angle$ 70 14'

Level in stream 132 ft from
2nd direction 510 east of N.

11.55
10.55
1.00

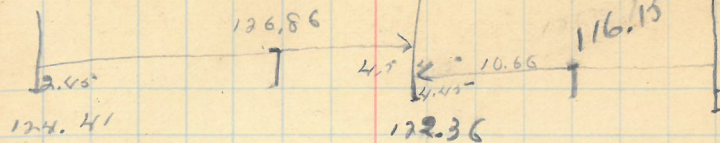
Levels on the St Augustine Road

Station	Distance	measured	actual
S.A.L.		182	126.15
29	2900-1/2 mi	265.2	209.4
77	7700-1 1/2 mi	268.2	213.4
97	9700-1 7/8 mi	272.6	216.8
132	13200-2 1/2	277.5	161.7
145	14500-2 3/4	274.5	218.7
182	18200-3 1/2	274.2	228.4
272	27200-5 1/8	272.8	217.0
278	27800-5 1/4	146.4	90.6
314	31400-6	133.1	77.3
337	35700-6 3/4	224.0	168.2
368	36900-7	145.7	89.9
39100	39100-7 3/8	181.5	123.7
494	49400-9 3/8	176.7	60.5
526	52600-10	111.8	56.0
556	55600-10 1/2	118.8	63.0
583	58300-11	104.1	48.3
631	63100-12	118.2	62.4
674	67400-12 3/4	94.2	38.4
720	72000-13 5/8	128.4	72.6

Assumed level S.A.L. by 182 =

182
176.157, 55.843
... as high.

Elevations at Jefferson Co line



Elevation to chub & tie up than 1
 Base City limit on river ^{elev.} 900

H.S.	H. 9	F.S.	actual elev.
3.65		5.95	109.35
5.75		5.40	109.70
11.00		.15	120.55
10.90		7.00	124.45
11.35		0.10	135.70
11.65		0.05	142.20
10.55		.30	152.55
10.75		0.05	168.25
10.70		0.14	178.81
12.11		0.40	190.52
7.50		11.70	186.32

the Boulders & Thompsons Peaks
 actual elev. 111.65

Turn of road

Bore on summit $82' 2.75" = 282.72$

Benton Colburn $82 = 274.76$

actual level is 186.41.

Leaves on Boulders road too high
 by $\frac{274.76}{186.41} 88.35$ ft.

Bench on N. Calhoun St. N End

uncut curb. Actual level 186.41

H.S. H.S

F.S

1.16 187.57

.25 187.26

11.64 198.90

.18 198.72

11.33 210.05

4.93 205.12

8.77 213.89

1.53 212.36

32.84

6.89

6.89

25.95

Bench on N. Calhoun St is 186.41

∴ Bench at City limits is 212.36

Bench on Colburn St. to Lewis Bank

Bench on Colburn St is actual 186.41

H.S.		F.S. Elev.	
11.60	198.01	0.02	197.99
8.50	206.49	4.88	201.61
1.59	202.20	7.40	194.80
3.44	198.24	3.00	195.24
11.07	206.31	0.28	206.03
10.03	216.06	.02	206.04
45.23		15.60	
15.60			
29.63			

Bench on Lewis Bank is 216.04
∴ Bench on Colburn St. is 186.41

Curb on W. side Adams St. to Lewis Bank

Level from Lake Jackson to
John Rollins Well. Sept 15, 1915

H.S.	H.Q.	Z.S.	Elev
2.82	152.30		
	3.66		170.76
∴ Elevation to well is			71.32
			18.32
			89.7 + 81

water in the well 114 ft from
Rock in this well at 78'
Actual level of Rock is 92.7
another well about 120 ft. N. W.
Retained water for a few years but
the other well, therefore well 114.6 in.
well dug on side of the
This 75 ft well was about
still another well dug near
went dry after a time.

B. W. Lake Jackson then at about 81.

$$\begin{array}{rcl}
 2.82 - .82 & = & 200\% \times 910 \times 10^\circ = \frac{6.82}{2.82} \\
 6.50 - 4.80 & = & 170\% \times 800 \times 40^\circ = \frac{71.32}{24.1} \\
 & & \frac{5.66}{18.44}
 \end{array}$$

to Surface.
Total depth 125'

Left 108 ft. Reached some rock
went dry. This well 11. ft 6 in lower.
to bottom of well from surface of 1st well,
hill 75 ft. stuck no rock.
 $\frac{71.32}{16.32}$
55 ft above the lake level. (Elev. partly Est.)
the lake 20 ft. no rock & also

Levels from Jones Bench on

H.S.	H. 2	F.S.	Elev.
9.45	111.71	1.49	110.22
4.20	114.42	7.70	on turnt. Campbell
6.90		8.75	at Rytrub.
2.80		8.35	"
2.75		4.10	"
5.60		1.93	"
9.33		3.85	"
3.96		6.94	"
44.99		43.11	"
43.11			"
1.88			"

Readings from Run # C. & B. Sum. 1/2

H.S.	H. 2	F.S.	Elev.
6.94	111.08	3.96	107.12
3.85	110.97	9.33	101.64
1.93	103.57	5.60	97.97
4.10	102.07	2.75	99.32
8.35	107.67	2.80	104.87
2.75	113.62	6.90	106.72
7.70	114.42	4.20	110.22
1.49	111.71	9.45	102.26

assumed 197.14 actual 102.26

Reading, Road Station 317+50

Distance 11.45 750 = 350 ft.

" 3.4 - (9.1 x 2) = 382 ft

" 6.65 - 170 = 495 ft

F.S. to lowest level 5 5.6

F.S. to Bench at top of old steps 2.62

H. 2 at lowest floor in road

F.S. 3.16 Tel. pole at Rytrub. top 1

Sound off post (1.45 from the ground) Elev.

Top of Rail of Rytrub. at same place 2.5

5.50 Elev.

B.M. C. & B. Sum. 104.14

B.M. Stat 317+50 of Jones.

Jones B.M. assumed 197.14
actual 102.26
difference 94.88 too high.

Bench on stump of south side of

H.S.	L. El.	orig. reading	8th Elev.	F.S.
4.8	4.9	F.S.		Elev.
9.45	111.71	14.9		110.92
11.20	114.42	2.62		111.08
4.92	116.00	0.40		
11.00		3.95		
1.10		6.00		
17.02		10.35		
10.35				
6.67				
4.25		9.65		
4.86		5.20		
			111.32	Lake Lake Sta

road at low place beyond Nickless.

B.M. on old stump of south of road.

Low ground of B.M. on stump 111.08 - 9.10 = 101.98
To Lake level 8.18 $\frac{10.35}{6.00} \angle 3^{\circ} 30' = \frac{86.5}{8.18} = 34.68$
 $\frac{24.85}{9.10} = 25.58$

level from Lake in

level of water in dam 12. Nelson is

$\frac{101.98}{20.35} = 26.40$

To Lake Nelson B.M. low of road

H.S.	L. El.	orig. reading	8th Elev.	F.S.
4.00	40'		10.3	
7.35			11.04	
			9.37	

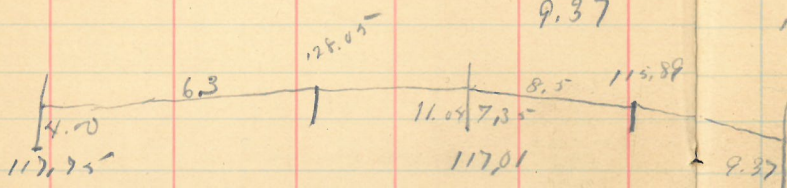
Lake Nelson station 112.75

Dist. 6.8 - 1.3 = 5.50 $\angle 40' = \frac{6.3}{4.0} = 1.575$

Dist 8.00 - 6.70 = 1.30 $\angle 3^{\circ} 45' = \frac{1.3}{1.03} = 1.262$

" 10.70 - 8.04 = 2.66 $\angle 5^{\circ} 30' = \frac{2.66}{1.03} = 2.583$

Lake at this stage 3.4 below bottom of dam of last house



Set 18 Level of Lake Hall

H.O	7.0	net. + sight	net. - sight
7.60		13.2	

2.25	20.15
------	-------

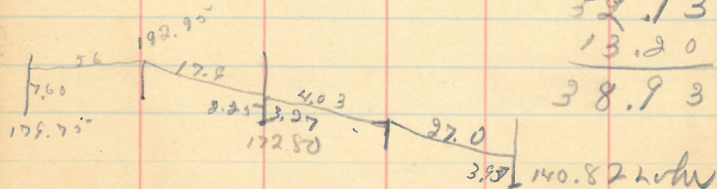
3.27	1.03
------	------

3.95	31.95
------	-------

52.13

13.20

38.93



B.M. N. End E. Head wall Sta 288

Assumed 167.38 actual + 12.36 = 179.75

9.70	- 5.50	= 420 ft	L	46°	=	5.6
------	--------	----------	---	-----	---	-----

3.95	- .50	345	L	30°	=	17.8
------	-------	-----	---	-----	---	------

3.96	- 2.58	= 138 ft	L	1048	=	4.3
------	--------	----------	---	------	---	-----

6.20	- 1.65	= 455 ft	L	3° 25'	=	1.03
------	--------	----------	---	--------	---	------

179.75

88.93

140.82 Lake Hall water level

22.0

30.85

Sept. 15. Level of Lake Jamonica
Elev.

H.S.	7.5
2.00	
6.18	9.33
6.53	2.05
5.70	8.25
6.02	10.54
26.44	8.74
	8.87

108.74
36.44
135.18
38.87
96.31

Octave

Bm. N. End of east headwall of Sta.

assumed 96.38 actual + 12.36 = 108.74

Electric 4.50 - 2.00 = 250' x 2 = 500 ft

9.33 - 6.28 = 313' x 2 = 626 ft.

Level of water in Lake Jamonica.

Bm N.E. Sta Headwall Station.

2.10	9.33
8.67	1.86

Elev. N.E. Main bridge as slope
108.22. Swamp level

about 98.22 at this bridge.

Level from Thurnmull Reef

F.S. F.S.

H.S.

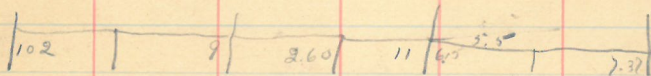
1.02 9.00

2.60 11.00

.65 7.37

2.67 21.60

6.94 48.97



Basin at Station 728+80 (15 mi.)

H.S. F.S.

7 11.2

4.14 9.1

5.09 7.23

9.23 16.33

Level of rock in well on

Bm. Station 925+85, 158.29+12.36

H.S.
0.37

to Lake MacBride Bay Sta. 442.

Bm. Assum. Elev, 169.91. actual 182.27

6.13 8.15 - 4.17 = 4.0 of L 48' = ^{5.15} 5.3

5.70 7.23 - 4.19 L 3' 4' = ^{15.8} 3.25
4.19
3.04 ft

Lake Level 140.24 ft.

Bm. on Claret Left 86.33+12.36 = 98.69

Level of land off the east is ^{98.69} 4.2
94.49

Level of water in this basin ^{98.69} 9.23
107.92
16.33
91.59

Hutelineon Place N of Lake Jormun
170.65 on Sweet Gum L 419 wal.

Elev. Rock on Thomomille Pool = non stat, line

Bm. Sta. 925 + 85 on S. line

H.S.	F.S.	170.65
0.37	5.8	10.36
<u>9.99</u>	<u>5.10</u>	181.01
10.36	10.90	10.90
		170.11

Level of second well same Bm

0.37	5.8	170.65
		10.36
<u>9.99</u>	<u>12.4</u>	181.01
10.36	18.2	181.2
		162.81

Third well same Bm

0.37	5.80	170.65
9.99	3.76	16.43
<u>6.07</u>	<u>9.48</u>	187.08
16.43	19.04	19.04
		168.04 ft

Level 158.29 + 12.36 = 170.65

5.82 1.50 = 430 x 2 = 860

170.65
58.29
112.36

Level of surface of well

11.2
12.3
12.47
3.4
8.8
12.3

Present depth of 2nd well 35.55 ft.

Said to have been dry Oct 50/2.

This report as to depth donated by Floyd.

162.81
50.00
112.81

Said to have been dry 84 ft.
no work depth measured by Floyd.

Said to have been covered since.

present depth 33 ft.

168.04
33.00
135.04

Level of surface of well.

Green Johnston

on Baker place on Bureau flatiron

along this well. David Walker

helped.

Sept 20

Level from Henry Thomas

H.S.	F.S.
4.40	10.65
.50	7.20
.92	6.98
3.45	9.20
1.780	9.10
2.20	9.10
13.27	32.23
	13.27
	38.96

well to Lake Jamonia

Sept 20 Prob 38

Actual level of surface of well

Level of limestone is

98
38.96
136.96
38.00
98.96

Level from Lick Damona to

H.S.	Ref	49.	F.S.	Ref	Elev.
10.82		107.13			
8.8		118.60			
2.60			9.4		109.80
2.2		132.61	6.59		123.41
			4.40		161.21
9.37		181.83			
			6.5		192.33
9.63		201.96	2.3		198.66
9.16		207.82	11.1		196.72
4.79		197.31	11.1		196.1
			5.14		184.67
7.05		191.22	10.25		181.47
6.21		187.68	5.6		182.08

well on Thompsons place E. 26

Bm on Bm on base line 107.13

10.68 - 8.10 = 2.58 L 2° 58' = 12.7

L 0

7.99 - 5.18 = 2.81 L 2° 25' = 11.42

3.9 - 7.0 = 3.1 L 2° 29' = 13.60

4.25 - 1.05 = 3.20 L 3° 45' = 26.00

6.4 - 2.4 = 4.00 L 4° 10' = 17.25

4.6 - 2.2 = 2.40 L 2° 35' = 17.00

8.4 - 4.6 = 3.80 L 0' 0"

6.1 - 3.45 = 2.65 L 55' down 42

6.1 - 3.45 = 2.65 L 1° 35' = 11.75

6.5 - 3.7 = 2.80 L

Well on rich line 46.5' deep.

Elev. Rich 184.67 - 46 = 138.67

0 0

0

Well 55' 6' deep

Inner and base line 10 ft.

Rich said to be at 20 ft.

Elev. Rich 182.08

44.1

137.98

Level of Obstruction of
Bridge on Bainbridge Road

8m below 7 ft high 183 =
Lowest Level of same place 176.6

Level corrected for lead 175.5 - 175.5
6.6 3.7
6.4 5.3

3.7 5.6
18.7 14.6

Lowest level = 171.6 ft. 3.5 4.7
24.2 19.3

Level of water 164.5 0. 4.0
24.2 23.3

Level of lead on
net steel 8 ft 184.8 ft

4.5
6.6

actual level 183. - 94.8 ft = 88.2

actual of lead 176.6 - 94.8 ft = 81.7

183.1 183.1
4.1 4.9
182.1 187.9
13.5 23.4
171.6 164.5 = actual river bottom 76.7
actual water level = 70

actual low level with 8 ft 89 ft

Level clay exposure at Station 520
on the Painted Rock. B.M. Below 1 low.
of low. Jaws and 207.2 = actual 113.4

actual

H.S. H. 9 F.S.

10.2 217.2 4.6

.85

6.45

7.28 - 5.6 = 1.68 L 30.50

1st clay at 207.2 + 5.6 = 212.8 ft. 116

2nd showing of clay 207.2 + 9.35 = 216.55 122

11.3 / 3rd down top of clay 127

127

Leads on clay just east of above
H.S. 9.2 122.6 + 3.0

Station above 510 B.M. some
Top of clay is 125.6 (actual).

Level on 5 m Hill

B.M. on Surt gun stump 10' to

Risp of Road at Sta Elev.

H.S. H. 9 F.S.

6.80 168.00

A.S. d.H. 8.3 - 5.4

= 290 L 20.35' = 13' + 6.85' = 19.85

5.94

Top of clay at level exposure.

Clay at highest Exp. 9.36 angle of Elev 10.16 - 8.54

= 162 ft = L 40.32' = 18.6 - 9.36 = 9.24

2.9

" " 5.20 - .63

= 457' L 30.5' = 24.6' - 2.9 = 21.7 - 2.9 =

9.68

.6

Top of Creek bedrock

and Bottom of lowest clay

Thickness of lowest clay

due off.

Merichman Road. Levels by
Sta Elev.

72	Flick news gate	207
	Depression not not. 3 M. P.	140
	Turn & Donalds place	224
	Depression of stream	100
	Low divide between streams	145
	Stream nearest Lake Jackson	96
	Hill Base Pine west of	
	Lopely place L of road	192.30

Barwood Beginning of 11+25 Elev. 156.68

M.P. 17. on AC.L. Foulw Branch &

strings well RM 182 ^{angle}

H.S	H. SL	H. SL	F.S.	F. SL	F. SL
4.60			4.00		0
6.55					0
			6.84	11.5	1.19
9.10			10.86		0
2.92				7.3	1.5
<u>23.19</u>			2.78		
			24.48		

M.P. on act 220 + Slough

H.S	F.S.	98.
4.15	3.80	

To water from tie on Bridge 9. H.
 From strings extreme high water 89
 1st lake reaching to 2nd day 2 " 96

Log of Mucicula N. 9 low

H.S	F.S	
2.77	3.28	1026
1.50	10.06	0

10 5. P1
 Elev. 24.

18.54
 4.75
24.29

307.91	179.75	
24.98	3.2	
281.79	9.34	182.45
	4.34	20.19
	5.00	172.80
		1.03
		2.9
182.	180.71	171.77
23.18	11.5	30.95
205.19		161.91
24.45		43
180.71	169.21	119.41
	7.3	
	161.91	
98.	103.85	102.15
102.15	1.280	3.80
	1.05	98.35
		2.00
		96.35

Water in muciculae slough. Low water
 Extreme high water in Lake Mucicula

BM T. 1st lake Bench. 222.12

$$\begin{array}{r}
 70.41 \\
 \underline{51.40} \\
 65.01 \\
 \underline{31.55} \\
 70.36 \\
 \underline{21.35} \\
 68.21 \\
 \underline{41.35} \\
 72.86 \\
 \underline{60.30} \\
 72.32 \\
 \underline{4.90} \\
 67.66 \\
 \underline{2.70} \\
 69.18 \\
 \underline{31.40} \\
 66.40
 \end{array}$$

$$\begin{array}{r}
 39 \quad 39 \\
 68 \quad 112 \\
 \underline{11711} \quad \underline{120} \\
 289 \\
 \underline{112} \\
 182
 \end{array}$$

$$\begin{array}{r}
 200 \\
 3 \\
 \hline
 200.82 \\
 \underline{3.65} \\
 197.17
 \end{array}$$

$$\begin{array}{r}
 199.4 \\
 \underline{197.1} \\
 2.3 \\
 327 \\
 \underline{317.30} \\
 9.67 \\
 12
 \end{array}$$

2.43

7.8 4.75
Bm. 197.14

2.77

$$\begin{array}{r}
 380 \\
 \underline{170} \\
 2102
 \end{array}$$

$$\begin{array}{r}
 458 \\
 \underline{170} \\
 270
 \end{array}$$

3.28

1' 26"

3' 6"

$$\begin{array}{r}
 77.16 \\
 \underline{5.0} \\
 82.16 \\
 \underline{4.85} \\
 77.31 \\
 \underline{9.2} \\
 74.11 \\
 \underline{5.70} \\
 68.41 \\
 \underline{9.65} \\
 78.06
 \end{array}$$

$$\begin{array}{r}
 78.06 \\
 \underline{3.55} \\
 75.51 \\
 \underline{10.2} \\
 86.41 \\
 \underline{9.90} \\
 76.51 \\
 \underline{9.65} \\
 86.16 \\
 \underline{9.20} \\
 82.86 \\
 \underline{5.06} \\
 87.86 \\
 \underline{10.85} \\
 77.01
 \end{array}$$

$$\begin{array}{r}
 76.51 \\
 \underline{9.65} \\
 86.16 \\
 \underline{9.20} \\
 82.86 \\
 \underline{5.06} \\
 87.86 \\
 \underline{10.85} \\
 77.01
 \end{array}$$

78.01

$$\begin{array}{r}
 78.01 \\
 \underline{6.80} \\
 81.11 \\
 \underline{3.40} \\
 76.51 \\
 \underline{4.1} \\
 72.41 \\
 \underline{9.65} \\
 81.06 \\
 \underline{4.65} \\
 76.41
 \end{array}$$

$$\begin{array}{r}
 76.41 \\
 \underline{6.30} \\
 82.71 \\
 \underline{8.25} \\
 80.56 \\
 \underline{3.45} \\
 84.01
 \end{array}$$

$$\begin{array}{r}
 80.56 \\
 \underline{3.45} \\
 84.01 \\
 \underline{10.30} \\
 79.71 \\
 \underline{4.05} \\
 77.76
 \end{array}$$

$$\begin{array}{r}
 77.76 \\
 \underline{10.17} \\
 67.68 \\
 \underline{3.85} \\
 70.83
 \end{array}$$

$$\begin{array}{r} 200.82 \\ 3.65 \\ \hline 197.17 \\ 3.75 \\ \hline 193.42 \end{array}$$

$$\begin{array}{r} 10.82 \\ 26408 \\ 3596 \\ \hline 4752 \end{array}$$

$$\begin{array}{r} 51480.00 \\ 11.7 \\ 9.0 \\ \hline 58.215 \\ 3.425 \\ \hline 63.640 \\ 4.160 \\ \hline 59.040 \\ 8.975 \\ \hline 68.015 \\ 7.150 \\ \hline 75.165 \\ 5.7 \\ \hline 80.865 \end{array}$$

4.8

$$\begin{array}{r} 10.65 \\ 15.55 \\ 2.11 \\ \hline 18.25 \\ 5.55 \\ \hline 23.80 \end{array}$$

$$\begin{array}{r} 200.53 \\ 15.53 \\ \hline 215.53 \\ 21.1 \\ \hline 194.43 \end{array}$$

48000

$$\begin{array}{r} 726.86 \\ 4.5 \\ \hline 122.36 \end{array}$$

$$\begin{array}{r} 116.71 \\ 9.45 \\ \hline 106.76 \end{array}$$

$$\begin{array}{r} 115.41 \\ 58.7 \\ \hline 56.7 \end{array}$$

$$\begin{array}{r} 9.7 \\ 11.0 \\ 1 \\ 3 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 4.02 \\ 3.17 \\ 7.1 \\ \hline 20.9 \end{array}$$

$$\begin{array}{r} 215.9 \\ 20.9 \\ 194.03 \end{array}$$

Temp'd ca 10k.

$$\begin{array}{r} 184.41 \\ 2.55 \\ \hline 126.86 \end{array}$$

$$\begin{array}{r} 106 \\ 8.67 \\ \hline 79.3 \end{array}$$

$$126.86$$

Gen

5.

$$\begin{array}{r} 4.25 \\ 2.45 \\ \hline 180 \\ 2 \\ \hline 4060 \end{array}$$

$$\begin{array}{r} 4.55 \\ 1.1 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 4.05 \\ 1.88 \\ \hline 3.97 \end{array}$$

$$\begin{array}{r} 22.9 \\ 26.2 \\ \hline 99.8 \\ 24.5 \\ \hline 5.3 \end{array}$$

$$131.26$$

$$\begin{array}{r} 117.33 \\ .8 \\ \hline 118.13 \end{array}$$

$$\begin{array}{r} 4.05 \\ 3.97 \\ \hline 8.02 \end{array}$$

$$\begin{array}{r} 218.13 \\ 3 \\ \hline 217.83 \\ 2.3 \\ \hline 215.53 \\ 13 \\ \hline 202.53 \end{array}$$

$$\begin{array}{r} 215.53 \\ 4.9 \\ \hline 210.63 \\ 8 \\ \hline 202.63 \end{array}$$

$$\begin{array}{r} 5280.75 \\ 6.75 \\ \hline 26400 \end{array}$$

$$\begin{array}{r} 215.53 \\ 21.68 \\ \hline 3564.00 \end{array}$$

$$\begin{array}{r} 194.43 \\ 4.20 \\ \hline 198.63 \end{array}$$

$$218.13$$

$$\begin{array}{r} 237.35 \\ 20.23 \\ \hline 22.12 \end{array}$$

Handwritten calculations on lined paper:

111

$$\begin{array}{r} 299.38 \\ 269.90 \\ \hline 30.118 \end{array}$$

$$\begin{array}{r} 274.76 \\ 295.25 \\ 269.90 \\ \hline 26.05 \end{array}$$

$$\begin{array}{r} 26.05 \\ 25.95 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 4.0 \\ 2.9 \\ \hline 1.1 \end{array}$$

$$\begin{array}{r} 4.25 \\ 2.06 \\ \hline 8.31 \end{array}$$

$$\begin{array}{r} 228. \\ 202.28 \\ \hline 26.72 \end{array}$$

$$\begin{array}{r} 197.68 \\ 197.68 \\ \hline 0 \end{array}$$

241.6

$$\begin{array}{r} 8.7 \\ 3.6 \\ \hline 12.30 \\ 18.85 \end{array}$$

$$\begin{array}{r} 80.325 \\ 15.45 \\ \hline 95.775 \\ 18.85 \\ \hline 114.625 \\ 21.58 \\ \hline 136.205 \end{array}$$

$$\begin{array}{r} 21 \cdot 6 \\ \underline{21 \cdot 2} \\ 2 \cdot 0 \end{array}$$
$$\begin{array}{r} 7.80 \\ 6.9 \overline{) 7.80} \\ \underline{6.9} \\ 0.90 \\ \underline{0.9} \\ 0.00 \end{array}$$

Stee 291.
 Bench on top of Stee
 feet on Lake Hall R
 also on headwall of culvert.
 at

9.45
 11.49
 1.91
 38.2

9.45
 7.10
 19.55
 3.20
 5.35

11.58
 6.27
 11.75
 7.50
 19.5
 5.35

19.5 - 12 x 2 =
 3.20
 7.45
 1.85
 11.30

50 N. 7. 2. 5. to 10. 5.
2. 4. 3.

$$\begin{array}{r}
 104.14 \\
 \times 2.11 \\
 \hline
 147.235 \\
 24.88 \\
 \hline
 102.26
 \end{array}$$

$$\begin{array}{r} 108.74 \\ 10.67 \\ \hline 119.41 \\ 11.12 \\ \hline 108.22 \end{array}$$

Level of Aveilla River

From River bottom to top of tie 9.3

From top of tie

H.S. F.S.

3.7 +.4

Level of River Profile to 9.3 + 2.7 + .4 =
13.4

Level of bottom of Grand Aveilla one
mile is about 13.5

Top of m.p. 130 is about 13.2 ft.
8

H.S.

4.18

2

12 ft.

Height of top of rail & river water

about 12 ft.

Tie with S.A.H. Profile. B.M.

S.A.H. water tank at Gallahome 80.268

H.S.	F.S.	80.268
4.18	1.85	92.8
3.0	1.55	90.068
4.8	3.50	86.568

190 ft or m.p. 165.
86.568
103.451 to high

3.7	234.76
	269.20
975	5.56
3.7	

665	420
420	245
245	3
490	

905.90	10.0
31.24	
274.76	

945	148
420	5.68
13.65	7.08
7.08	
6.57	

Profile from Dist.
2

105.90	19.54	19.54
	4.76	11.76
	24.29	31.24

117.75
10.3
128.05
11.04
117.01

8.5
7.35
1.15

2 32

* 62

128.05

117.01

115.86

25

9.37

34.35
81.56

11.70

$$\begin{array}{r} 1.45 \\ 75.4 \times 12 \\ \hline 9.12 \\ 134.12 \\ \hline 1.45 \\ \hline 11.70 \end{array}$$

$$\begin{array}{r} 2.67 \\ 150.47 \\ \hline 150.47 \\ \hline 150.47 \end{array}$$

$$\begin{array}{r} 1803 \\ 12.55 \\ \hline 12.55 \\ \hline 12.55 \end{array}$$

$$\begin{array}{r} 6.8 \\ 13.50 \\ \hline 13.50 \\ \hline 13.50 \end{array}$$

$$\begin{array}{r} 6.8 \\ 13.50 \\ \hline 13.50 \\ \hline 13.50 \end{array}$$

$$\begin{array}{r} 150.47 \\ 1.45 \\ \hline 150.47 \\ \hline 150.47 \end{array}$$

0.05

11.15

48

2.65 top of 1st clay

2.8

4.05

2.65 top of 2nd clay

11.05

2.83

5.48

6.88

18.03

clay on west side rd 12.0

$$\begin{array}{r} 23 \\ 5.47 \\ \hline 27.5 \end{array}$$

$$\begin{array}{r} 150.47 \\ 27 \\ \hline 123 \end{array}$$

143

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Instrument Makers,
And Dealers in
SCIENTIFIC BOOKS,
TROY, N. Y.

