



6/24/2016

Ms. Cindy Mulkey
Florida Department of Environmental Protection
Siting Office
2600 Blair Stone Road
Tallahassee, Florida 32399-3000

Re: Seminole Electric Cooperative, Inc.
Midulla Generating Station, Hardee County Florida
Power Plant Certification No. PA89-25F
Post-Certification Amendment to Application

Dear Ms. Mulkey:

Pursuant to Section 403.5113(1)(a), Florida Statutes and Rule 62-17.205, Florida Administrative Code, please accept this letter and attachments as a post-certification amendment to the Seminole Electric Cooperative, Inc. ("Seminole") Site Certification Application ("Application") for the Midulla Generating Station in Hardee County, Florida. This post-certification amendment addresses the installation of a new 9ft x 12ft security booth with entrance road modification, as well as a containment area for sodium hypochlorite unloading.

The new security booth will be located in the center of the current entrance road, which is already an impervious surface. The new entrance road will require widening a portion of the current road and result in an increase of asphalt by 2,430 square feet (ft²). The removal of the existing security booth and restroom will reduce the impervious area by 192 ft². (See figure 1 of the attached report).

The proposed containment area for sodium hypochlorite unloading will be adjacent to an existing sodium hypochlorite tank near the northwest portion of the MGS site within the service water pretreatment area (see figure 2 of the attached report). The containment area would help to control incidental spills during unloading operations. The size of the containment area will be 13ft x 15ft, with a 4 inch berm.

The proposed entrance road modification and unloading containment area will result in an increased impervious surface total of approximately 2,433 ft². 2,238 ft² is from the modified entrance road minus the old security booth/restroom that will be removed. 195 ft² is from the installation of the proposed sodium hypochlorite containment area. Both areas eventually drain into an onsite 4.28-acre stormwater detention pond. To ensure that the existing pond has sufficient storage capacity to attenuate the runoff from the new impervious surface, IBC Consulting conducted the stormwater analysis that is attached below. Based on the results of the stormwater analysis, the existing stormwater treatment system has sufficient storage and attenuation capacity to accommodate the entrance road modification and the sodium hypochlorite unloading containment area.

If the Department concurs, Seminole requests that this letter and its attachments be forwarded to all appropriate agencies and parties to the original certification proceeding as a permissible post-certification amendment to the Application. If you or any of the parties have any questions or concerns, or require additional information, please contact me at (813) 963-0994, ext. 1281.

Sincerely,



Michael Lee
Senior Environmental
Regulatory Coordinator

Cc: Lewis Snyder, SECI
David Childs, HG&S

IBC Consulting

4126 NW 66th Terrace
Gainesville FL 32606
352-256-1883
ivanbchou@gmail.com

June 22, 2016

Mr. Michael Lee
Seminole Electric Cooperative, Inc.
P.O. Box 272000
Tampa, Florida 33688-2000

Re: Seminole Electric Cooperative Inc.'s Midulla Generating Station (MGS)
Stormwater Analysis for Entrance Road Modification and Sodium Hypochlorite
Unloading Containment

Dear Michael:

I am submitting this report to present the results of a hydraulic/hydrological analysis to assess the hydrological effects of the proposed constructions at the Seminole Electric Cooperative Inc. (SECI) Richard J. Midulla Generating Station (MGS), including the entrance road modification and a containment area for sodium hypochlorite unloading.

PROJECT DESCRIPTION

1. Currently, there is a small 8-ft-by-8-ft security booth located at the south side (exit lane) of the MGS entrance road. The security guard has to walk across the exit lane to check in visitors, which can be a safety concern. SECI plans to widen a portion of the entrance road and construct a new 9-ft-by-12-ft security booth located in the center of the entrance road between the entrance and exit lanes so the security guard can check visitors in and out without stepping onto the road. This larger climate-controlled guardhouse, with a restroom, will house various types of electronic equipment to comply with the North American Electric Reliability Corporation (NERC) Critical Infrastructure Protection (CIP) physical security standard. The existing 8-ft-by-8-ft security booth, along with a 12-ft-by-12-ft concrete slab that the booth sits on, will be demolished. An adjacent 6-ft-by-8-ft restroom will be demolished also. The configuration of the modified entrances road is shown in Figure 1. The road widening will increase the asphalt surface by 2,430 square feet (ft²). The removal of the existing security booth and the restroom will reduce the impervious area by 192 ft².
2. There is an existing sodium hypochlorite tank near the northwest portion of the MGS site within the service water pretreatment area. SECI plans to construct a concrete-paved unloading area, with the containment berm, adjacent to the tank to control incidental spills during unloading operations. In the event of an incidental spill, the spilled chemical will be contained, cleaned up, and transported to an approved disposal/treatment site by approved contractors. The size of the containment area will be 13 ft by 15 ft, and the height of the containment berm will be 4 inches. The location of the proposed containment area is shown in Figure 2.

The proposed entrance road modification and the proposed unloading containment area will result in increased impervious surface area and, thus, more stormwater runoff, which drains into an onsite 4.28-acre stormwater detention pond. To ensure the existing pond has sufficient storage capacity to attenuate the runoff from the new impervious surfaces, IBC Consulting (IBC) conducted the stormwater analysis presented herein.

HYDROLOGICAL AND HYDRAULIC ANALYSIS

In 2004, Environmental Consulting & Technology, Inc. (ECT) conducted a stormwater management study (ECT, 2004)¹ for the construction of peaker units on the MGS site and subsequently obtained the permits for the peaker project. The drainage basin delineation of the MGS site area presented in ECT's previous study was used and modified for this analysis.

Figure 3 presents the drainage basin delineation of the MGS facility, and Figure 4 depicts the drainage pattern. Appendix A contains the construction drawings of the stormwater management system. The proposed entrance road modification (in Basin 5B) will slightly shift the sub-basin boundary. The proposed unloading containment (in Basin 5C) will not change the basin boundary. The total drainage basin area of the MGS site within the stormwater management system is 47.22 acres. To identify land use cover and compute the curve numbers (CN) of the sub-basins, an aerial photograph flown on January 17, 2016 was obtained (Figure 5).

The areas covered by buildings, concrete, asphalt, gravel, and grass are determined using the recent aerial photograph and onsite investigation (Figure 5). Subsequently, CNs were calculated (Appendix B) based on hydrologic soil conditions and the land use distribution after the proposed installation of the entrance road modification, unloading containment, and the switchyard house addition.

The following subsections provide a description of each sub-basin.

SUB-BASIN 1A

Currently, Sub-basin 1A is an open area that was originally used as a construction laydown area during the construction of the peaker units. A limestone base was constructed in a majority of the sub-basin area to provide a stable base for construction equipment staging and an asphalt road was constructed to provide access to the combustion turbines. Since that time, grass has grown and is well established in this area, making it much more pervious. A 12-ft-by-12-ft concrete pad that supports the security booth and a 6-ft-by-8-ft restroom will be demolished and replaced by grass coverage (Figure 1). The CN calculation for Sub-basin 1A reflects the demolition of the security booth and the restroom.

SUB-BASIN 1B

The majority of Sub-basin 1B is the power block for the peaker project combustion turbines (CTs) and substation. Ground cover is predominately gravel and buildings. The transformers sit in three containment areas with 58-inch-high concrete containment walls. Rainfall on

¹ Environmental Consulting & Technology, Inc. (ECT). 2004. Stormwater Management Report for Payne Creek Generating Station Peaker Project, ECT No. 030790-0100. August.

these containment areas is pumped to and treated by an oil/water separator, then discharged into a 570-acre cooling water reservoir and does not drain into the stormwater pond. The total area of the transformer containment is 2,772 ft².

SUB-BASIN 1C

Land cover within Sub-basin 1C primarily consists of dense grass. A small gravel-covered gas metering and gas regulating station is located in the sub-basin.

SUB-BASIN 1D

Sub-basin 1D consists of a grassy area and a drainage channel.

SUB-BASIN 3

The plant's substation for the CT units is located within this sub-basin, and the majority of the land cover is gravel. Similar to Sub-basin 1B, there are two concrete containments with 18.5-inch-high concrete walls that enclose the transformer equipment. Rainfall on these 2,778-ft² areas is pumped to and treated by an oil/water separator then discharged into a 570-acre cooling water reservoir, which has a permitted National Pollutant Discharge Elimination System (NPDES) outfall.

SUB-BASIN 4

Sub-basin 4 is the combined-cycle site, and the land cover is mainly concrete and gravel. An ammonia hydroxide tank is located within a 798-ft² containment area with a 48-inch high concrete wall. A 12.5-ft-by-57-ft unloading area with a 6-inch containment berm is adjacent to the tank containment. The design storm is 8.4 inches (25-year, 24-hour event). Therefore, the unloading containment can contain 71 percent of the design rainfall. As a reasonable approximation, 71 percent of the unloading area is considered to be containment and 29 percent of the unloading area is considered to be concrete without containing berms. The total area of the tank containment and unloading containment, as used by the hydrological analysis, is 1,307 ft². Rainfall on these containment areas is pumped to and treated by an oil/water separator, then discharged into a 570-acre cooling water reservoir.

SUB-BASIN 5A

Sub-basin 5A was originally used as construction parking area during the peaker project construction. Since that time, grass has grown into this area, making it somewhat more pervious. A portion of this area is now used for contractor parking.

SUB-BASIN 5B

The existing land use consists of two warehouse buildings, equipment storage area, and open space (grass). A large portion of Sub-basin 5B was originally designated as a construction laydown area. However, only a small portion of this planned laydown area is currently used. A lubricating oil building was constructed in 2011 in this sub-basin. In an area south of the fuel oil storage tanks, there are five concrete containment basins (total of 1,131 ft² with various containment depths) that enclose fuel pumps. There is also a 2,905 ft² fuel unloading area with a 6.5-inch-high containment berm and two floor drains. The floor of the fuel unloading area is graded with slopes to allow rainwater to drain toward the floor drains at the lower locations. It was estimated that the unloading containment area has the

capacity to contain at least 7 inches of rainfall. Comparing to the design storm of 8.4 inches, these areas are equivalent to a deep containment of 3,438 ft². Rainfall onto these containment areas is pumped to and treated by an oil/water separator and is discharged into a 570-acre cooling water reservoir.

SUB-BASIN 5C

A truck turnaround and demineralized water tank are in Sub-basin 5C along with two water tanks and a treatment facility. The rest of this sub-basin is open space (grass). As shown in Figure 2, a proposed sodium hypochlorite unloading containment area (13 ft by 15 ft) will be located in this basin. This unloading area will be enclosed by a 4-inch berm. The design storm (25-year, 24-hour event) is 8.4 inches. Therefore, the unloading containment can contain 48 percent of the design rainfall. In the event of an incidental spill, the spilled chemical will be contained, cleaned up, and transported to an approved disposal/treatment site by approved contractors.

SUB-BASIN 6

Sub-basin 6 includes a substation, an administrative building, and a water treatment building. The land cover in this area is mainly concrete and gravel. In 2011, SECI obtained a permit to construction a 19-ft-by-38-ft (722 ft²) free-standing roof between the contractor service building and water treatment building. This permitted structure has not been built to date. In August 2015, SECI submitted a post-certification amendment request to install a 20-ft-by-20-ft concrete monolithic slab to support the switchyard control house addition. The CN calculation for Sub-basin 6 includes the switchyard control house addition and the not-yet-built roof. Similar to Sub-basins 1B and 3, there are three containments with 18.5-inch concrete walls that enclose the transformer equipment. Rainfall on these 2,777-ft² areas is pumped to and treated by an oil/water separator, then discharged into a 570-acre cooling reservoir.

SUB-BASIN 7 AND 7A

This area includes three fuel tanks within containment berms. Rainfall onto these two sub-basins is pumped and treated by an oil/water separator then is discharged into a 570-acre cooling reservoir, an NPDES wastewater system. Stormwater is contained within the bermed area and released to the cooling reservoir. Therefore, the area within the containment berm (3.7 acres) was not considered in the detention pond analysis.

SUB-BASIN 8

Sub-basin 8 includes an existing 4.28-acre stormwater pond. The bottom elevation of the existing stormwater pond is 114 feet referenced to the National Geodetic Vertical Datum (ft-NGVD). The control structure of the detention pond includes a 4-inch bleed-down orifice (at elevation 120 ft-NGVD), a 15-ft overflow weir (at elevation 121.1 ft-NGVD), and a 100-ft emergency spillway (at elevation 123.0 ft-NGVD). The top elevation of the berm around the detention pond is 125 ft-NGVD. Appendix A presents the construction drawings of the control structure. Table 1 provides the stage-area-volume information for the stormwater pond.

Table 1. Stage-Area-Volume Information for the Stormwater Detention Pond

Stage (ft-NGVD)	Area (acre)	Volume (ac-ft)
114	1.58	0.00
115	0.52	1.05
116	1.80	2.21
117	1.91	4.06
118	2.29	6.16
119	2.98	8.80
120	3.43	12.00
121	3.60	15.52
122	3.76	19.20
123	3.93	23.04
124	4.10	27.06
125	4.28	31.25

Source: ECT, 2012.

SUB-BASIN 9

Sub-basin 9 includes a truck turnaround area. It is mostly grass with some asphalt. This basin is a deep depressional area. It is a self-contained, isolated basin and does not drain to the 4.28-acre stormwater pond.

Among the total drainage area of 47.22 acres, the total containment area, or isolated basins, is 4.84 acres. Therefore, only 42.38 acres of the drainage area actually drains into the stormwater pond.

Table 2 lists the CN values determined for each sub-basin that drains into the stormwater pond. The CNs for Sub-basins 1A, 5B, 5C, and 6 include the proposed constructions and demolitions.

Table 2. Post-Construction Stormwater Sub-basin Weighted Average CNs

Sub-basin ID	Sub-basin Area (acres)	Weighted Average CN (Post-Construction)
1A	3.15	89.3
1B	7.65	93.9
1C	4.48	83.5
1D	1.00	81.7
3	2.66	91.4
4	2.09	93.7
5A	4.19	85.7
5B	4.67	87.1
5C	3.48	86.8
6	3.61	92.9
8	<u>5.38</u>	<u>95.6</u>
Composite	42.38*	90.0

*4.84 acres of containment area is not included.

ECT (2004) reported a pre-development (pre-MGS) drainage basin area of 44.8 acres, which was incorrect, probably because of the less accurate mapping technique used at the time. The correct basin size is 47.22 acres, which is consistent with the post-development

drainage basin area. A weighted average CN of 84.6 was used for pre-development runoff modeling. The land use distribution and the weighted average CNs for the pre- and post-development sub-basins are presented in Appendix B.

RESULTS

The Interconnected Channel and Pond Routing Model (ICPR) was used to compute the surface runoff and discharge hydrograph for the pre- and post-development conditions under a 25-year, 24-hour storm event (8.4 inches). According to the 36-hour drawdown requirement [Section 5.2.a.5 of Southwest Florida Water Management District's (SWFWMD's) Basis of Review], a 36-hour drawdown elevation of 120.77 ft-NGVD was computed by the ICPR and used as the initial water level condition for flood routing. Appendix C contains the model inputs/outputs. According to the model results, the peak discharge under the pre-construction conditions is 90.02 cubic feet per second (cfs). The post-development peak discharge from the stormwater pond under a 25-year, 24-hour storm event is 78.94 cfs. The post-construction peak discharge is less than the pre-development discharge. Therefore, the peak flow requirement is met.

SWFWMD's stormwater rules (Section 5.2.a.1, Basis of Review) requires that the stormwater detention pond should have a water quality treatment capacity of 1 inch of runoff from the contributing drainage area. The required water quality treatment volume was calculated to be 3.53 acre-ft, based on the 42.38-acres drainage area contributing to the pond. The stormwater pond at MGS has a water quality treatment capacity between elevations 120 ft-NGVD and 121.1 ft-NGVD. Based on the interpolation of Table 1, the stormwater pond has a water quality treatment capacity of 3.89 acre-ft, which is greater than the required water quality treatment volume of 3.53 acre-ft. The 120-hour drawdown water level in the stormwater pond computed by ICPR is 120.22 ft-NGVD. Therefore, the quality treatment volume is discharged in no less than 120 hours, which complies with Section 5.2.a.4 of the Basis of Review. The 60-hour drawdown water level in the stormwater pond computed by ICPR is 120.58 ft-NGVD. The 60-hour drawdown volume, based on Table 1, is 1.9 acre-ft, less than one-half of the quality treatment volume capacity, which also complies with Section 5.2.a.4 of the Basis of Review. Therefore, the treatment volume requirement is met.

The ICPR model results indicate that the peak water level in the stormwater pond under a 25-year, 24-hour storm event is 122.98 ft-NGVD, which allows approximately 2.02 ft. of freeboard in the pond. Under a 100-year, 24-hour storm event (10.5 inches), the ICPR simulated peak water elevation in the pond is 123.39 ft-NGVD. All of the plant infrastructures at MGS are above elevation 128 ft-NGVD, therefore the plant facility and personnel are protected from 100-year flood.

Based on the results of this stormwater analysis, the existing stormwater treatment system has sufficient storage and attenuation capacity to accommodate the entrance road modification and the sodium hypochlorite unloading containment.

DISCUSSION

The stormwater analysis by ECT (2004) and the subsequent hydrological analyses by ECT for minor site modifications had considered Sub-basin 9 as a self-contained, isolated basin. The security guard, whose workplace is only 200-ft from Sub-basin 9, indicated that the road

2430 - new road
- 192 - all groundwater
2238
195 sq ft for containment

in the area had never been flooded. Therefore, it was a reasonable assertion that Sub-basin 9 is an isolated basin, even though there had been no infiltration test data to technically verify this claim. A sensitivity analysis was conducted to evaluate the hydrological effects of Sub-basin 9, if it were to be included in ICPR model. In this sensitivity analysis, Sub-basin 9 (0.83 acres) was included in the model and was assigned a worst case CN value of 100. The result of this sensitivity analysis with the inclusion of Sub-basin 9 under the worst case condition under a 25-year 24 hour storm indicated that the peak discharge from the stormwater pond would be 81.08 cfs, which is still less than the pre-development peak discharge of 90.02 cfs.

CONCLUSION

The results of the hydrological/hydraulic analysis indicate that the existing stormwater pond has sufficient capacity to provide both water quality and quantity treatment for the proposed entrance road modification and the sodium hypochlorite unloading containment.

Appendix D provides the operation and maintenance plan of the stormwater management system.

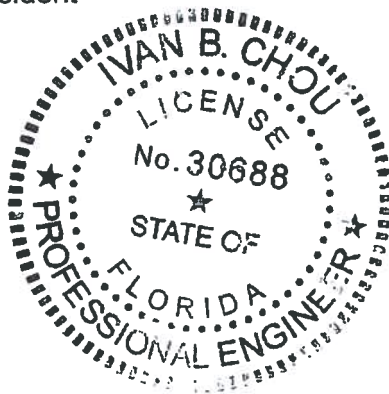
Please let me know if you have any questions regarding this stormwater analysis.

Sincerely,

IBC CONSULTING



Ivan B. Chou, P.E. No 30688
President

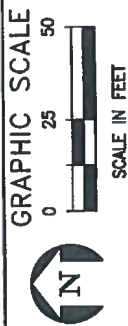


June 22, 2016

Date

cc: Justin Gostnell
Robert Burleson

Attachment



LEGEND

Expanded Road (2,430 sq.ft.)

30' MOTOR OPERATED
SLIDE GATE

NEW FENCE

EXISTING ROAD

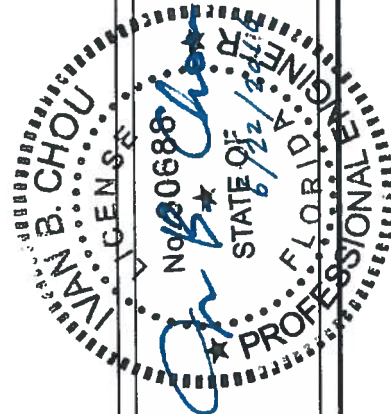
NEW SECURITY BOOTH

EXISTING SECURITY BOOTH
AND RESTROOM TO BE DEMOLISHED

FIGURE 1.

**PROPOSED ENTRANCE ROAD MODIFICATION
MIDULLA STATION**

Source: SECI, 2016; IBC consulting, 2016.



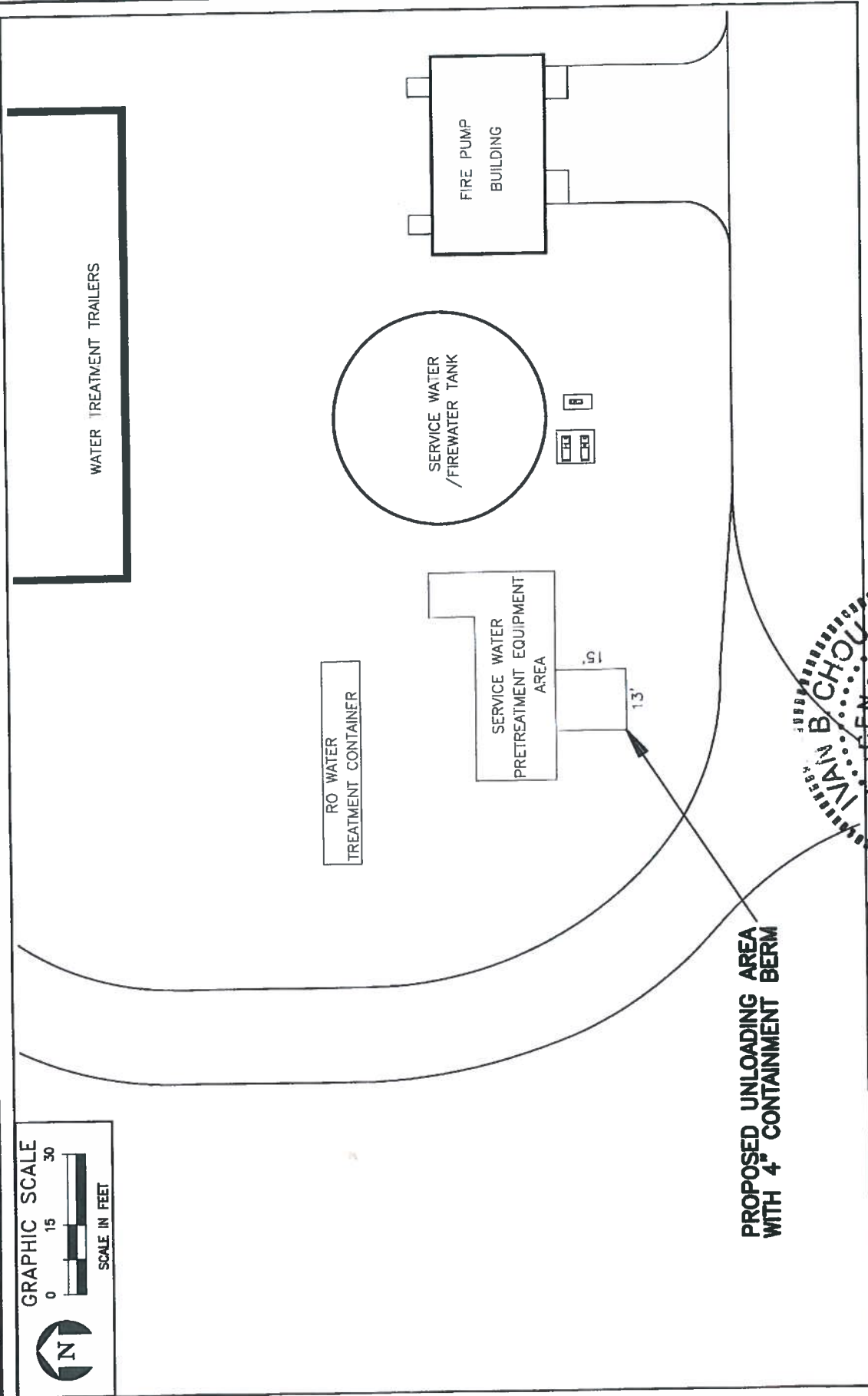
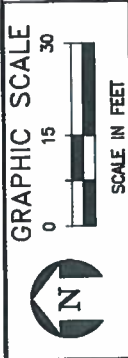


FIGURE 2.
UNLOADING CONTAINMENT
MIDULLA STATION
Source: SECI, 2016; IBC consulting, 2016.

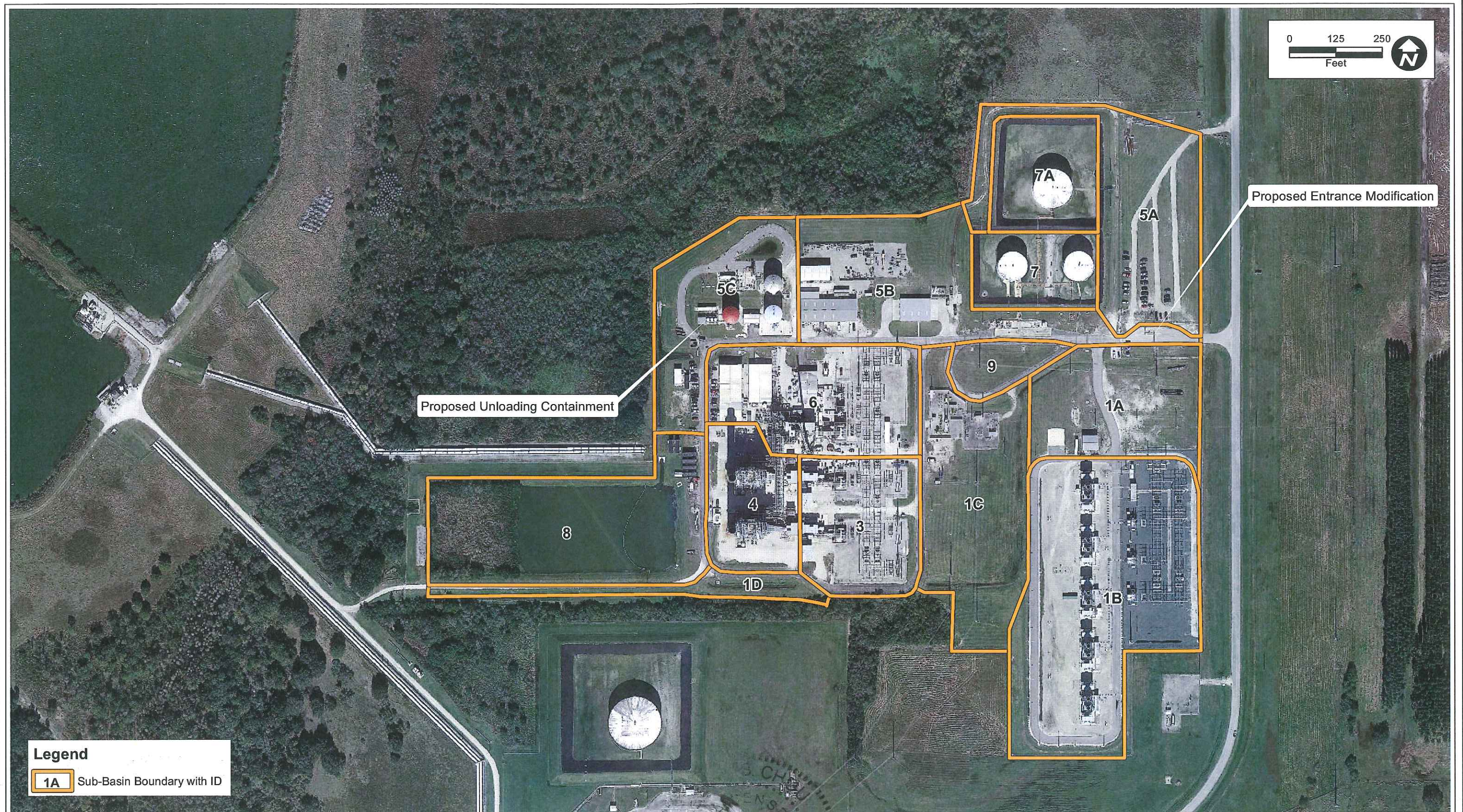
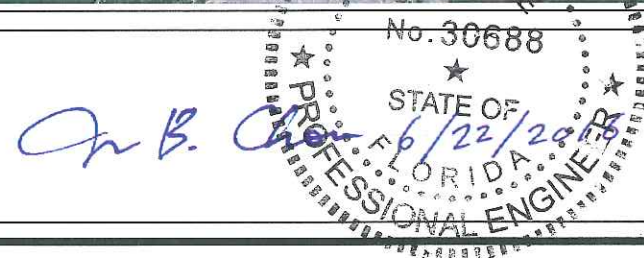


FIGURE 3.
AERIAL MAP
MIDULLA GENERATING STATION

Sources: Google Earth, 2016; ECT, 2012; IBC, 2016; DMC, 2016



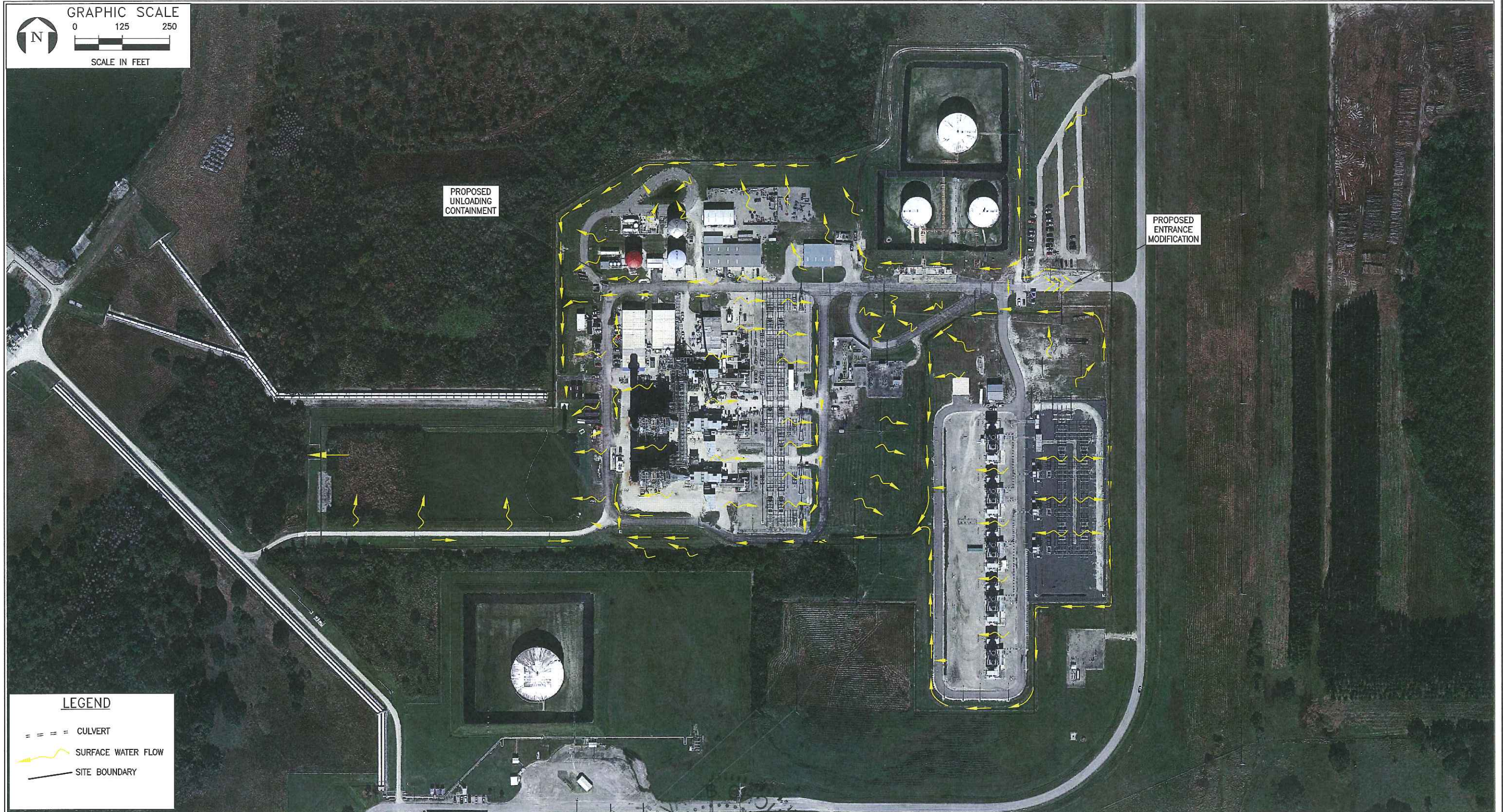


FIGURE 4.
DRAINAGE PATTERN
MIDULLA GENERATING STATION

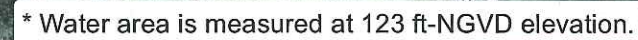
Source: Google Earth, 2016; ECT, 2012; IBC, 2016; DMC, 2016.

Professional Engineer
No. 30688
STATE OF FLORIDA
6/22/2016

Seminole Electric
COOPERATIVE, INC.
IN PARTNERSHIP WITH THOSE WE SERVE

0 125 250
Feet





Sources: Google Earth, 2016; ECT, 2012; IBC, 2016; DMC, 2016

No. 30688

STATE OF
FLORIDA
PROFESSIONAL ENGINEER

6/22/2017

J. B. Ch...

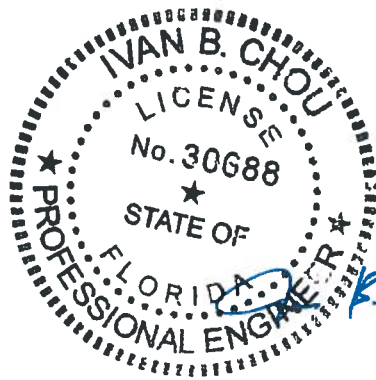
Appendix A

Construction Drawings of the Stormwater Management System



Appendix B

Curve Number Computations



Ivan B. Chou

6/7/2016

Runoff curve number - Pre-development

Project MGS	By IBC	Date 6/2/2016
Location Bowling Green, Fl	Checked RWB	Date 6/2/016

Check one: ☒ Present ☐ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area ☒ acres ☐ mi ² ☐ %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
D	Slough	85			15.5983	1325.9
D	Flatwood	80			24.7676	1981.4
D	Marsh & Pond	100			6.8506	685.1
Totals ➡					47.2165	3992.3235

¹ Use only one CN source per line

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{3992.324}{47.2165} = 84.55357$ Use CN ➡ **84.554**

2. Runoff

Frequency	Storm #1	Storm #2	Storm #3
25 yr	25 yr		
Rainfall, P (24-hour)	8.4		
Runoff, Q	6.55		

(Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)

Post-development Runoff curve number - Basin 1A

Project MGS Entrance Road and Unloading Containmen		By IBC		Date 6/2/2016	
Location Bowling Green, Fl		Checked RWB		Date 6/2/016	

Check one: ☐ Present ☒ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4	☒ acres ☐ mi ² ☐ %	
D	Asphalt	98			0.3037	29.8
D	Mature grass over limerock	88			2.6376	232.1
D	Building and Concrete	98			0.0781	7.7
D	Gravel	91			0.1331	12.1
Totals ➡					3.1525	281.6

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{281.6373}{3.1525} = 89.33776$ Use CN ➡ **89.338**

2. Runoff

Frequency yr Rainfall, P (24-hour) in Runoff, Q in (Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>Storm #1</th> <th>Storm #2</th> <th>Storm #3</th> </tr> <tr> <td>25 yr</td> <td> </td> <td> </td> </tr> <tr> <td>8.4</td> <td> </td> <td> </td> </tr> <tr> <td>7.12</td> <td> </td> <td> </td> </tr> </table>	Storm #1	Storm #2	Storm #3	25 yr			8.4			7.12		
Storm #1	Storm #2	Storm #3											
25 yr													
8.4													
7.12													

Post-development Runoff curve number - Basin 1B

Project MGS Entrance Road and Unloading Containmen	By IBC	Date 6/2/2016
Location Bowling Green, Fl	Checked RWB	Date 6/2/016

Check one: ☐ Present ☒ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area ☒ acres ☐ mi ² ☐ %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
D	Asphalt	98			0.8740	85.7
D	Building and concrete	98			0.7285	71.4
D	Sod	80			0.8714	69.7
D	Gravel*	95			5.1770	491.8

¹ Use only one CN source per line

Totals ➡

7.6509 718.6

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{718.572}{7.6509} = 93.91993$ Use CN ➡ **93.920**

* Gravel was placed over existing limerock area therefore the curve number for limerock will be used

2. Runoff

Frequency	Storm #1	Storm #2	Storm #3
..... yr	25 yr		
Rainfall, P (24-hour)	8.4		
..... in	7.67		
Runoff, Q			
..... in			

(Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)

Post-development Runoff curve number - Basin 1C

Project MGS Entrance Road and Unloading Containmen		By IBC		Date 6/2/2016	
Location Bowling Green, Fl		Checked RWB		Date 6/2/016	

Check one: ☐ Present ☒ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area ☒ acres ☐ mi ² ☐ %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
D	Gravel	91			0.2333	21.2
D	Asphalt	98			0.7103	69.6
D	Sodded area	80			3.5166	281.3
D	Building and Concrete	98			0.0209	2.0
Totals ➡					4.4811	374.2

¹ Use only one CN source per line

CN (weighted)
$$= \frac{\text{total product}}{\text{total area}} = \frac{374.2159}{4.4811} = 83.50983$$
 Use CN ➡ **83.510**

2. Runoff

Frequency	Storm #1	Storm #2	Storm #3
Rainfall, P (24-hour)	25 yr		
Runoff, Q	8.4		
	6.42		

(Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)

Post-development Runoff curve number - Basin 1D

Project MGS Entrance Road and Unloading Containmen		By IBC		Date 6/2/2016	
Location Bowling Green, Fl		Checked RWB		Date 6/2/016	

Check one: ☐ Present ☒ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area ☒ acres ☐ mi ² ☐ %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
D	Asphalt	98			0.0712	7.0
D	Sodded area	80			0.8868	70.9
D	Gravel	91			0.0418	3.8
Totals ➡					0.9998	81.7

¹ Use only one CN source per line

CN (weighted)
$$= \frac{\text{total product}}{\text{total area}} = \frac{81.7254}{0.9998} = 81.74175$$
 Use CN ➡ **81.742**

2. Runoff

Frequency	Storm #1	Storm #2	Storm #3
Rainfall, P (24-hour)	25 yr		
Runoff, Q	8.4		
	6.21		

(Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)

Post-development Runoff curve number - Basin 3

Project MGS Entrance Road and Unloading Containmen	By IBC	Date 6/2/2016
Location Bowling Green, Fl	Checked RWB	Date 6/2/016

Check one: ☐ Present ☒ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area ☒ acres ☐ mi ² ☐ %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
D	Gravel	91			1.7156	156.1
D	Asphalt	98			0.2981	29.2
D	Sodded area	80			0.3144	25.2
D	Building and Concrete	98			0.3327	32.6

¹ Use only one CN source per line

Totals ➡

2.6608 243.1

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{243.09}{2.6608} = 91.35974$ Use CN ➡ **91.360**

2. Runoff

Frequency yr
Rainfall, P (24-hour) in
Runoff, Q in

Storm #1	Storm #2	Storm #3
25 yr		
8.4		
7.36		

(Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)

Post-development Runoff curve number - Basin 4

Project MGS Entrance Road and Unloading Containmen		By IBC		Date 6/2/2016	
Location Bowling Green, Fl		Checked RWB		Date 6/2/016	

Check one: ☐ Present ☒ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area ☒ acres ☐ mi2 ☐ %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
D	Building and concrete	98			0.8722	85.5
D	Asphalt	98			0.2057	20.2
D	Sodded area	80			0.1679	13.4
D	Gravel	91			0.8487	77.2
Totals ➡					2.0945	196.3

CN (weighted)
$$= \frac{\text{total product}}{\text{total area}} = \frac{196.2979}{2.0945} = 93.72065$$
 Use CN ➡ **93.721**

* included existing and expanded area

2. Runoff

Frequency yr Rainfall, P (24-hour) in Runoff, Q in (Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>Storm #1</th> <th>Storm #2</th> <th>Storm #3</th> </tr> <tr> <td>25 yr</td> <td> </td> <td> </td> </tr> <tr> <td>8.4</td> <td> </td> <td> </td> </tr> <tr> <td>7.65</td> <td> </td> <td> </td> </tr> </table>	Storm #1	Storm #2	Storm #3	25 yr			8.4			7.65		
Storm #1	Storm #2	Storm #3											
25 yr													
8.4													
7.65													

Post-development Runoff curve number - Basin 5A

Project MGS Entrance Road and Unloading Containmen		By IBC		Date 6/2/2016	
Location Bowling Green, Fl		Checked RWB		Date 6/2/016	

Check one: ☐ Present ☒ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4	☒ acres ☐ mi ² ☐ %	
D	Gravel	91			0.4648	42.3
D	Grass/gravel	85			3.7281	316.9
Totals ➡					4.1929	359.2

¹ Use only one CN source per line

CN (weighted)
$$= \frac{\text{total product}}{\text{total area}} = \frac{359.1853}{4.1929} = 85.66512$$
 Use CN ➡ **85.665**

2. Runoff

Frequency yr Rainfall, P (24-hour) in Runoff, Q in (Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>Storm #1</th> <th>Storm #2</th> <th>Storm #3</th> </tr> <tr> <td>25 yr</td> <td> </td> <td> </td> </tr> <tr> <td>8.4</td> <td> </td> <td> </td> </tr> <tr> <td>6.68</td> <td> </td> <td> </td> </tr> </table>	Storm #1	Storm #2	Storm #3	25 yr			8.4			6.68		
Storm #1	Storm #2	Storm #3											
25 yr													
8.4													
6.68													

Post-development Runoff curve number - Basin 5B

Project MGS Entrance Road and Unloading Containmen	By IBC	Date 6/2/2016
Location Bowling Green, Fl	Checked RWB	Date 6/2/016

Check one: ☐ Present ☒ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area ☒ acres ☐ mi ² ☐ %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
D	Buildings and concrete	98			0.4681	45.9
D	Gravel	91			1.1680	106.3
D	Sodded area	80			2.3855	190.8
D	Asphalt	98			0.6518	63.9

¹ Use only one CN source per line

Totals ➡

4.6734 406.9

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{406.8782}{4.6734} = 87.06257$

Use CN ➡

87.063

2. Runoff

Frequency yr
Rainfall, P (24-hour) in
Runoff, Q in

Storm #1	Storm #2	Storm #3
25 yr		
8.4		
6.85		

(Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)

Post-development Runoff curve number - Basin 5C

Project MGS Entrance Road and Unloading Containmen		By IBC		Date 6/2/2016		
Location Bowling Green, Fl		Checked RWB		Date 6/2/016		
Check one: ☐ Present ☒ Developed						
1. Runoff curve number						
Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area ☒ acres ☐ mi ² ☐ %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
D	Gravel	91			0.2456	22.3
D	Buildings, tanks, and concrete	98			0.3402	33.3
D	Asphalt	98			0.8190	80.3
D	Sodded area	80			2.0763	166.1
¹ Use only one CN source per line					Totals ➡	3.4811 302.1
CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{302.0552}{3.4811} = 86.77004$ Use CN ➡ 86.770						
* Includes 1 proposed tank and 2 existing						
2. Runoff						
Frequency		Storm #1	Storm #2	Storm #3		
Rainfall, P (24-hour)		25 yr				
Runoff, Q		8.4				
		6.81				
(Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)						

Post-development Runoff curve number - Basin 6

Project MGS Entrance Road and Unloading Containmen		By IBC		Date 6/2/2016	
Location Bowling Green, Fl		Checked RWB		Date 6/2/016	

Check one: ☐ Present ☒ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area ☒ acres ☐ mi ² ☐ %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
D	Asphalt	98			0.5336	52.3
D	Buildings/concrete	98			0.8469	83.0
D	Sodded area	80			0.2417	19.3
D	Gravel	91			1.9862	180.7

¹ Use only one CN source per line

Totals ➡	3.6084	335.4
-----------------	--------	-------

CN (weighted)
$$= \frac{\text{total product}}{\text{total area}} = \frac{335.3692}{3.6084} = 92.94125$$
 Use CN ➡ **92.941**

2. Runoff

Frequency	Storm #1	Storm #2	Storm #3
25 yr			
Rainfall, P (24-hour)	8.4		
Runoff, Q	7.55		

(Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)

Post-development Runoff curve number - Basin 8

Project MGS Entrance Road and Unloading Containmen		By IBC		Date 6/2/2016	
Location Bowling Green, Fl		Checked RWB		Date 6/2/016	

Check one: ☐ Present ☒ Developed

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹			Area ☒ acres ☐ mi ² ☐ %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
D	Water *	100			3.9325	393.3
D	Asphalt	98			0.1455	14.3
D	Sodded area	80			1.0724	85.8
D	Gravel	91			0.2339	21.3
D						
D						
Totals ➡					5.3843	514.6

Use only one CN source per line

CN (weighted)
$$= \frac{\text{total product}}{\text{total area}} = \frac{514.5859}{5.3843} = 95.57155$$
 Use CN ➡ **95.572**

* Water area is measured at 123 ft-NGVD elevation.

2. Runoff

Frequency	Storm #1	Storm #2	Storm #3
25 yr	25 yr		
Rainfall, P (24-hour)	8.4		
Runoff, Q	7.87		

(Use P and CN with table 2-1, figure 2-1, or equations 2-3 and 2-4)

Appendix C

ICPR Model Input/Output

Robert Whaley Burleson
06 JUNE 2016

SECI MGS Site
Pre-Development Scenario
Input Summary

=====

Basins

```

Name: MGS Site Pre      Node: MGS Site      Status: Onsite
Group: BASE             Type: SCS Unit Hydrograph CN

Unit Hydrograph: Uh323      Peaking Factor: 323.0
Rainfall File: Flmod        Storm Duration(hrs): 24.00
Rainfall Amount(in): 8.400  Time of Conc(min): 72.00
Area(ac): 47.216           Time Shift(hrs): 0.00
Curve Number: 84.55        Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00

```

=====

Nodes

```

Name: MGS Site          Base Flow(cfs): 0.000      Init Stage(ft): 120.000
Group: BASE             Warn Stage(ft): 121.000
Type: Time/Stage

```

Time(hrs)	Stage(ft)
0.00	120.000
30.00	120.000

=====

Hydrology Simulations

```

Name: MGS Pre
Filename: C:\Users\rburleson\Desktop\Projects\SECI\ICPR Simulations\Pre\MGS Pre.R32

Override Defaults: Yes
Storm Duration(hrs): 24.00
Rainfall File: Flmod
Rainfall Amount(in): 8.40

```

Time(hrs)	Print Inc(min)
30.000	5.00

SECI MGS Site
Pre-Development Scenario
Basin Output Summary

Basin Name: MGS Site Pre
Group Name: BASE
Simulation: MGS Pre
Node Name: MGS Site
Basin Type: SCS Unit Hydrograph

Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 9.60
Comp Time Inc (min): 5.00
Rainfall File: Flmod
Rainfall Amount (in): 8.400
Storm Duration (hrs): 24.00
Status: Onsite
Time of Conc (min): 72.00
Time Shift (hrs): 0.00
Area (ac): 47.216
Vol of Unit Hyd (in): 1.001
Curve Number: 84.554
DCIA (%): 0.000

Time Max (hrs): 12.75
Flow Max (cfs): 90.02
Runoff Volume (in): 6.540
Runoff Volume (ft3): 1120996

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

=====

Basins
=====

Name: Basin 1A	Node: Areal	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh323		
Rainfall File: Flmod	Peaking Factor: 323.0	
Rainfall Amount (in): 8.400	Storm Duration (hrs): 24.00	
Area (ac): 3.152	Time of Conc (min): 10.00	
Curve Number: 89.34	Time Shift (hrs): 0.00	
DCIA (%): 0.00	Max Allowable Q (cfs): 999999.000	

Name: Basin 1B	Node: Area 1B	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh323		
Rainfall File: Flmod	Peaking Factor: 323.0	
Rainfall Amount (in): 8.400	Storm Duration (hrs): 24.00	
Area (ac): 7.651	Time of Conc (min): 10.00	
Curve Number: 93.92	Time Shift (hrs): 0.00	
DCIA (%): 0.00	Max Allowable Q (cfs): 999999.000	

Name: Basin 1C	Node: Areal	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh323		
Rainfall File: Flmod	Peaking Factor: 323.0	
Rainfall Amount (in): 8.400	Storm Duration (hrs): 24.00	
Area (ac): 4.481	Time of Conc (min): 37.00	
Curve Number: 83.51	Time Shift (hrs): 0.00	
DCIA (%): 0.00	Max Allowable Q (cfs): 999999.000	

Name: Basin 1D	Node: Area 1D	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh323		
Rainfall File: Flmod	Peaking Factor: 323.0	
Rainfall Amount (in): 8.400	Storm Duration (hrs): 24.00	
Area (ac): 1.000	Time of Conc (min): 32.00	
Curve Number: 81.74	Time Shift (hrs): 0.00	
DCIA (%): 0.00	Max Allowable Q (cfs): 999999.000	

Name: Basin 3	Node: Area 3	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

Unit Hydrograph: Uh323
Rainfall File: Flmod
Rainfall Amount (in): 8.400
Area (ac): 2.661
Curve Number: 91.36
DCIA(%): 0.00
Peaking Factor: 323.0
Storm Duration (hrs): 24.00
Time of Conc (min): 10.00
Time Shift (hrs): 0.00
Max Allowable Q (cfs): 999999.000

Name: Basin 4
Group: BASE
Node: Area 4
Type: SCS Unit Hydrograph CN
Status: Onsite

Unit Hydrograph: Uh323
Rainfall File: Flmod
Rainfall Amount (in): 8.400
Area (ac): 2.095
Curve Number: 93.72
DCIA(%): 0.00
Peaking Factor: 323.0
Storm Duration (hrs): 24.00
Time of Conc (min): 10.00
Time Shift (hrs): 0.00
Max Allowable Q (cfs): 999999.000

Name: Basin 5A
Group: BASE
Node: Area 5A
Type: SCS Unit Hydrograph CN
Status: Onsite

Unit Hydrograph: Uh323
Rainfall File: Flmod
Rainfall Amount (in): 8.400
Area (ac): 4.193
Curve Number: 85.67
DCIA(%): 0.00
Peaking Factor: 323.0
Storm Duration (hrs): 24.00
Time of Conc (min): 10.00
Time Shift (hrs): 0.00
Max Allowable Q (cfs): 999999.000

Name: Basin 5B
Group: BASE
Node: Area 5B
Type: SCS Unit Hydrograph CN
Status: Onsite

Unit Hydrograph: Uh323
Rainfall File: Flmod
Rainfall Amount (in): 8.400
Area (ac): 4.673
Curve Number: 87.06
DCIA(%): 0.00
Peaking Factor: 323.0
Storm Duration (hrs): 24.00
Time of Conc (min): 42.00
Time Shift (hrs): 0.00
Max Allowable Q (cfs): 999999.000

Name: Basin 5C
Group: BASE
Node: Area 5C
Type: SCS Unit Hydrograph CN
Status: Onsite

Unit Hydrograph: Uh323
Rainfall File: Flmod
Rainfall Amount (in): 8.400
Area (ac): 3.481
Curve Number: 86.77
DCIA(%): 0.00
Peaking Factor: 323.0
Storm Duration (hrs): 24.00
Time of Conc (min): 32.00
Time Shift (hrs): 0.00
Max Allowable Q (cfs): 999999.000

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

 Name: Basin 6 Node: Area 6 Status: Onsite
 Group: BASE Type: SCS Unit Hydrograph CN

 Unit Hydrograph: Un323 Peaking Factor: 323.0
 Rainfall File: F1mod Storm Duration(hrs): 24.00
 Rainfall Amount(in): 8.400 Time of Conc(min): 10.00
 Area(ac): 3.608 Time Shift(hrs): 0.00
 Curve Number: 92.94 Max Allowable Q(cfs): 999999.000
 DCIA(\$): 0.00

 Name: Basin 8 Node: POND Status: Onsite
 Group: BASE Type: SCS Unit Hydrograph CN

 Unit Hydrograph: Un323 Peaking Factor: 323.0
 Rainfall File: F1mod Storm Duration(hrs): 24.00
 Rainfall Amount(in): 8.400 Time of Conc(min): 14.00
 Area(ac): 5.384 Time Shift(hrs): 0.00
 Curve Number: 95.57 Max Allowable Q(cfs): 999999.000
 DCIA(\$): 0.00

=====

Name: A Base Flow(cfs): 0.000 Init Stage(ft): 122.000
 Group: BASE Warn Stage(ft): 129.000
 Type: Stage/Area

Stage(ft) Area(ac)

 Name: AA Base Flow(cfs): 0.000 Init Stage(ft): 121.000
 Group: BASE Warn Stage(ft): 128.500
 Type: Stage/Area

Stage(ft) Area(ac)

 Name: Area 1B Base Flow(cfs): 0.000 Init Stage(ft): 126.000
 Group: BASE Warn Stage(ft): 127.500
 Type: Stage/Area

Stage(ft) Area(ac)

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

Name: Area 1D Group: BASE Type: Stage/Area	Base Flow(cfs): 0.000	Init Stage(ft): 122.000 Warn Stage(ft): 128.500
Stage(ft)	Area(ac)	
Name: Area 3 Group: BASE Type: Stage/Area	Base Flow(cfs): 0.000	Init Stage(ft): 126.000 Warn Stage(ft): 128.500
Stage(ft)	Area(ac)	
Name: Area 4 Group: BASE Type: Stage/Area	Base Flow(cfs): 0.000	Init Stage(ft): 126.000 Warn Stage(ft): 128.500
Stage(ft)	Area(ac)	
Name: Area 5A Group: BASE Type: Stage/Area	Base Flow(cfs): 0.000	Init Stage(ft): 129.000 Warn Stage(ft): 133.000
Stage(ft)	Area(ac)	
Name: Area 5B Group: BASE Type: Stage/Area	Base Flow(cfs): 0.000	Init Stage(ft): 125.000 Warn Stage(ft): 129.000
Stage(ft)	Area(ac)	
Name: Area 5C Group: BASE Type: Stage/Area	Base Flow(cfs): 0.000	Init Stage(ft): 122.000 Warn Stage(ft): 128.500
Stage(ft)	Area(ac)	

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

Name: Area 6
Group: BASE
Type: Stage/Area
Base Flow(cfs): 0.000
Init Stage(ft): 125.000
Warn Stage(ft): 128.500

Stage(ft) Area(ac)

Name: AREA 9
Group: BASE
Type: Stage/Area
Base Flow(cfs): 0.000
Init Stage(ft): 127.000
Warn Stage(ft): 129.500

Stage(ft) Area(ac)

Name: Areal
Group: BASE
Type: Stage/Area
Base Flow(cfs): 0.000
Init Stage(ft): 127.000
Warn Stage(ft): 129.000

Stage(ft) Area(ac)

Name: L
Group: BASE
Type: Stage/Area
Base Flow(cfs): 0.000
Init Stage(ft): 121.000
Warn Stage(ft): 128.500

Stage(ft) Area(ac)

Name: Outfall
Group: BASE
Type: Time/Stage
Base Flow(cfs): 0.000
Init Stage(ft): 119.000
Warn Stage(ft): 121.000

Time(hrs) Stage(ft)
0.00 119.000
30.00 120.000

Name: POND
Group: BASE
Type: Stage/Area
Base Flow(cfs): 0.000
Init Stage(ft): 120.770
Warn Stage(ft): 125.500

Stage(ft) Area(ac)

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

119.800 3.4320
121.000 3.5950
122.000 3.7610
123.000 3.9300
124.000 4.1020
125.000 4.2770

```

=====
Name: P-10      From Node: AA      Length(ft): 100.00
Group: BASE      To Node: POND      Count: 2
Friction Equation: Average Conveyance
Solution Algorithm: Automatic
Flow: Both
Entrance Loss Coef: 0.40
Exit Loss Coef: 1.00
Bend Loss Coef: 0.00
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dn
Stabilizer Option: None
=====

```

Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

```

=====
Name: P-11      From Node: AREA 9   Length(ft): 30.00
Group: BASE      To Node: Area1     Count: 1
Friction Equation: Average Conveyance
Solution Algorithm: Automatic
Flow: Both
Entrance Loss Coef: 0.40
Exit Loss Coef: 1.00
Bend Loss Coef: 0.00
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dn
Stabilizer Option: None
=====

```

Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Name: P-3 From Node: Area 3 Length(ft): 30.00
Group: BASE To Node: A Count: 1

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

UPSTREAM	DOWNSTREAM	Friction Equation: Average Conveyance
Geometry: Circular	Circular	Solution Algorithm: Automatic
Span(in): 24.00	24.00	Flow: Both
Rise(in): 24.00	24.00	Entrance Loss Coef: 0.40
Invert(ft): 122.500	122.300	Exit Loss Coef: 1.00
Manning's N: 0.013000	0.013000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dn
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Name: P-4	From Node: Area 4	Length(ft): 30.00
Group: BASE	To Node: Area 1D	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Average Conveyance
Geometry: Circular	Circular	Solution Algorithm: Automatic
Span(in): 24.00	24.00	Flow: Both
Rise(in): 24.00	24.00	Entrance Loss Coef: 0.40
Invert(ft): 122.300	122.000	Exit Loss Coef: 1.00
Manning's N: 0.013000	0.013000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dn
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Name: P-5	From Node: L	Length(ft): 110.00
Group: BASE	To Node: POND	Count: 2
UPSTREAM	DOWNSTREAM	Friction Equation: Average Conveyance
Geometry: Circular	Circular	Solution Algorithm: Automatic
Span(in): 36.00	36.00	Flow: Both
Rise(in): 36.00	36.00	Entrance Loss Coef: 0.40
Invert(ft): 120.300	120.000	Exit Loss Coef: 1.00
Manning's N: 0.013000	0.013000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dn
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Name: PNEW
Group: BASE

From Node: A
To Node: Area 1D

Length(ft): 300.00
Count: 2

Friction Equation: Average Conveyance
Solution Algorithm: Automatic

Flow: Both

Entrance Loss Coef: 0.40
Exit Loss Coef: 1.00
Bend Loss Coef: 0.00
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dn
Stabilizer Option: None

UPSTREAM
Circular
Span(in): 36.00
Rise(in): 36.00
Invert(ft): 123.000
Manning's N: 0.013000
Top Clip(in): 0.000
Bot Clip(in): 0.000

DOWNSTREAM
Circular
Span(in): 36.00
Rise(in): 36.00
Invert(ft): 121.700
Manning's N: 0.013000
Top Clip(in): 0.000
Bot Clip(in): 0.000

Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Name: C-15A
Group: BASE

From Node: Area 5A
To Node: Area 5B

Length(ft): 425.00
Count: 1

UPSTREAM
Trapezoidal
Invert(ft): 128.000
Top Clip(ft): 9999.000
Manning's N: 0.025000
Bot Clip(ft): 0.000
Main XSec:
AuxElev1(ft):
Aux XSec1:
AuxElev2(ft):
Aux XSec2:
Top Width(ft):
Depth(ft):
Bot Width(ft): 5.000
LtsdSlp(h/v): 3.00
RtsdSlp(h/v): 3.00

DOWNSTREAM
Trapezoidal
Invert(ft): 125.000
Top Clip(ft): 9999.000
Manning's N: 0.025000
Bot Clip(ft): 0.000

Friction Equation: Average Conveyance
Solution Algorithm: Automatic

Flow: Both

Contraction Coef: 0.000
Expansion Coef: 0.000
Entrance Loss Coef: 0.000
Exit Loss Coef: 0.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dn
Stabilizer Option: None

Name: C-15B
Group: BASE

From Node: Area 5B
To Node: Area 5C

Length(ft): 620.00
Count: 1

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

UPSTREAM	DOWNSTREAM	Friction Equation: Average Conveyance
Geometry: Trapezoidal	Trapezoidal	Solution Algorithm: Automatic
Invert(ft): 124.800	121.900	Flow: Both
TCIPinitz(ft): 9999.000	9999.000	Contraction Coef: 0.000
Manning's N: 0.025000	0.025000	Expansion Coef: 0.000
Top Clip(ft): 0.000	0.000	Entrance Loss Coef: 0.000
Bot Clip(ft): 0.000	0.000	Exit Loss Coef: 0.000
Main XSec:		Outlet Ctrl Spec: Use dc or tw
AuxElev1(ft):		Inlet Ctrl Spec: Use dn
Aux XSec1:		Stabilizer Option: None
AuxElev2(ft):		
Aux XSec2:		
Top Width(ft):		
Depth(ft):	6.000	
Bot Width(ft):	3.00	
LtSdSlp(h/v):	3.00	
RtSdSlp(h/v):	3.00	

Name: C-15C From Node: Area 5C Length(ft): 200.00
Group: BASE To Node: AA Count: 1

UPSTREAM	DOWNSTREAM	Friction Equation: Average Conveyance
Geometry: Trapezoidal	Trapezoidal	Solution Algorithm: Automatic
Invert(ft): 122.000	121.000	Flow: Both
TCIPinitz(ft): 9999.000	9999.000	Contraction Coef: 0.000
Manning's N: 0.032000	0.032000	Expansion Coef: 0.000
Top Clip(ft): 0.000	0.000	Entrance Loss Coef: 0.000
Bot Clip(ft): 0.000	0.000	Exit Loss Coef: 0.000
Main XSec:		Outlet Ctrl Spec: Use dc or tw
AuxElev1(ft):		Inlet Ctrl Spec: Use dn
Aux XSec1:		Stabilizer Option: None
AuxElev2(ft):		
Aux XSec2:		
Top Width(ft):		
Depth(ft):	8.000	
Bot Width(ft):	3.00	
LtSdSlp(h/v):	3.00	
RtSdSlp(h/v):	3.00	

Name: C-16 From Node: Area 6 Length(ft): 85.00
Group: BASE To Node: Area 5C Count: 1

UPSTREAM	DOWNSTREAM	Friction Equation: Average Conveyance
Geometry: Trapezoidal	Trapezoidal	Solution Algorithm: Automatic
Invert(ft): 122.000	121.900	Flow: Both
TCIPinitz(ft): 9999.000	9999.000	Contraction Coef: 0.000
Manning's N: 0.032000	0.032000	Expansion Coef: 0.000
Top Clip(ft): 0.000	0.000	Entrance Loss Coef: 0.000
Bot Clip(ft): 0.000	0.000	Exit Loss Coef: 0.000
Main XSec:		Outlet Ctrl Spec: Use dc or tw
AuxElev1(ft):		Inlet Ctrl Spec: Use dn
Aux XSec1:		Stabilizer Option: None
AuxElev2(ft):		
Aux XSec2:		

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

Top Width(ft) :
Depth(ft) :
Bot Width(ft) : 8.000
LtsdSlp(h/v) : 3.00
RtsdSlp(h/v) : 3.00

Name: C-1A From Node: Areal Length(ft): 510.00
Group: BASE To Node: Area 1B Count: 1

DOWNSTREAM
Geometry: Trapezoidal
Invert(ft) : 126.000
TCLPInitz(ft) : 9999.000
Manning's N : 0.025000
Top Clip(ft) : 0.000
Bot Clip(ft) : 0.000
Main XSec:
AuxElev1(ft) :
AuxElev2(ft) :
Aux XSec1:
Aux XSec2:
Top Width(ft) :
Depth(ft) :
Bot Width(ft) : 8.000
LtsdSlp(h/v) : 3.00
RtsdSlp(h/v) : 3.00

Friction Equation: Average Conveyance
Solution Algorithm: Automatic
Flow: Both
Contraction Coef: 0.000
Expansion Coef: 0.000
Entrance Loss Coef: 0.000
Exit Loss Coef: 0.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dn
Stabilizer Option: None

Name: C-1B From Node: Area 1B Length(ft): 270.00
Group: BASE To Node: A Count: 1

DOWNSTREAM
Geometry: Trapezoidal
Invert(ft) : 124.000
TCLPInitz(ft) : 9999.000
Manning's N : 0.025000
Top Clip(ft) : 0.000
Bot Clip(ft) : 0.000
Main XSec:
AuxElev1(ft) :
AuxElev2(ft) :
Aux XSec1:
Aux XSec2:
Top Width(ft) :
Depth(ft) :
Bot Width(ft) : 8.000
LtsdSlp(h/v) : 3.00
RtsdSlp(h/v) : 3.00

Friction Equation: Average Conveyance
Solution Algorithm: Automatic
Flow: Both
Contraction Coef: 0.000
Expansion Coef: 0.000
Entrance Loss Coef: 0.000
Exit Loss Coef: 0.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dn
Stabilizer Option: None

Name: C-7 From Node: Area 1D Length(ft): 270.00
Group: BASE To Node: L Count: 1

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

UPSTREAM	DOWNSTREAM	Friction Equation: Average Conveyance
Geometry: Trapezoidal	Trapezoidal	Solution Algorithm: Automatic
Invert (ft): 122.500	121.000	Flow: Both
TCIP1n12 (ft): 9999.000	9999.000	Contraction Coef: 0.000
Manning's N: 0.032000	0.032000	Expansion Coef: 0.000
Top Clip (ft): 0.000	0.000	Entrance Loss Coef: 0.000
Bot Clip (ft): 0.000	0.000	Exit Loss Coef: 0.000
Main XSec:		Outlet Ctrl Spec: Use dc or tw
AuxElev1 (ft):		Inlet Ctrl Spec: Use dn
Aux XSec1:		Stabilizer Option: None
AuxElev2 (ft):		
Aux XSec2:		
Top Width (ft):		
Depth (ft):		
Bot Width (ft): 8.000	8.000	
LtSdslp(h/v): 3.00	3.00	
RtSdslp(h/v): 3.00	3.00	

=====

==== Drop Structures =====

=====

Name: control struct From Node: POND Length(ft): 24.00
Group: BASE To Node: Outfall Count: 3

UPSTREAM	DOWNSTREAM	Friction Equation: Average Conveyance
Geometry: Circular	Circular	Solution Algorithm: Automatic
Span(in): 36.00	36.00	Flow: Both
Rise(in): 36.00	36.00	Entrance Loss Coef: 0.400
Invert(ft): 119.700	119.600	Exit Loss Coef: 1.000
Manning's N: 0.013000	0.013000	Outlet Ctrl Spec: Use dc or tw
Top Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dn
Bot Clip(in): 0.000	0.000	Solution Incs: 10

Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall

*** Weir 1 of 3 for Drop Structure control struct ***

UPSTREAM	DOWNSTREAM	TABLE
Count: 1	Bottom Clip(in): 0.000	
Type: Horizontal	Top Clip(in): 0.000	
Flow: Both	Weir Disc Coef: 3.200	
Geometry: Circular	Orifice Disc Coef: 0.600	
Span(in): 4.00	Invert(ft): 120.000	
Rise(in): 4.00	Control Elev(ft): 120.000	

*** Weir 2 of 3 for Drop Structure control struct ***

UPSTREAM	DOWNSTREAM	TABLE
Count: 1	Bottom Clip(in): 0.000	
Type: Vertical: Mavis	Top Clip(in): 0.000	
Flow: Both	Weir Disc Coef: 3.200	
Geometry: Rectangular	Orifice Disc Coef: 0.600	

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

Span(in): 180.00 Invert(ft): 121.100
Rise(in): 36.00 Control Elev(ft): 121.100

*** Weir 3 of 3 for Drop Structure control struct ***

TABLES

Count: 1 Bottom Clip(in): 0.000
Type: Vertical: Fread Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
Span(in): 1200.00 Invert(ft): 123.000
Rise(in): 48.00 Control Elev(ft): 123.000

=====

Name: 100yrpro
Filename: C:\Users\rburleson\Desktop\Projects\SECI\ICPR Simulations\Post-Development\100yr.R32

Override Defaults: Yes
Storm Duration(hrs): 24.00
Rainfall File: Flmod
Rainfall Amount(in): 10.50

Time(hrs)	Print Inc(min)
13.000	15.00
18.000	5.00
36.000	15.00

Name: 25yrpro
Filename: C:\Users\rburleson\Desktop\Projects\SECI\ICPR Simulations\Post-Development\POST25.R32

Override Defaults: Yes
Storm Duration(hrs): 24.00
Rainfall File: Flmod
Rainfall Amount(in): 8.40

Time(hrs)	Print Inc(min)
13.000	15.00
18.000	5.00
36.000	15.00

=====

Name: 100 yr post Hydrology Sim: 100yrpro
Filename: C:\Users\rburleson\Desktop\Projects\SECI\ICPR Simulations\Post-Development\100yr Post.I32

Execute: Yes Restart: No Patch: No
Alternative: No

Max Delta Z(ft): 1.00 Delta Z Factor: 0.00500
Time Step Optimizer: 0.000

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard
Control House Addition
Input Summary

Start Time (hrs): 0.000 End Time (hrs): 36.00
Min Calc Time (sec): 0.0000 Max Calc Time (sec): 0.0000
Boundary Stages:
Boundary Flows:

Time (hrs) Print Inc (min)

36.000 15.000
Group Run

BASE Yes

Name: 25 yr post Hydrology Sim: 25yrpro
Filename: C:\Users\zburleson\Desktop\Projects\SECI\ICPR Simulations\Post-Development\25yr post.i32

Execute: Yes Restart: No Patch: No
Alternative: No

Max Delta Z (ft): 1.00 Delta Z Factor: 0.00500
Time Step Optimizer: 0.000
Start Time (hrs): 0.000 End Time (hrs): 36.00
Min Calc Time (sec): 0.0000 Max Calc Time (sec): 0.0000
Boundary Stages:
Boundary Flows:

Time (hrs) Print Inc (min)

36.000 15.000
Group Run

BASE Yes

MGS Entrance Road Modification, Sodium Hypochlorite Unloading Containment, and Switchyard Control House Addition
Node Min/Max Report

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
A	BASE	100 Yr post	12.15	126.571	129.000	-0.3000	3998	130.346	12.13	85.243
AA	BASE	100 Yr post	12.16	123.880	128.500	-0.0049	2579	66.689	12.16	66.645
Area 1B	BASE	100 Yr post	12.15	126.595	127.500	0.0043	9918	80.688	0.00	105.962
Area 1D	BASE	100 Yr post	12.28	124.633	128.500	-0.0048	3420	100.373	12.13	99.612
Area 3	BASE	100 Yr post	12.08	127.194	128.500	0.0050	115	17.610	0.00	24.385
Area 4	BASE	100 Yr post	0.00	126.000	128.500	-0.0050	119	14.040	0.00	26.593
Area 5A	BASE	100 Yr post	0.00	129.000	133.000	-0.0050	2390	26.526	0.00	26.752
Area 5B	BASE	100 Yr post	12.07	125.990	129.000	0.0036	6816	38.764	11.91	41.295
Area 5C	BASE	100 Yr post	12.16	123.968	128.500	0.0035	8378	210.190	12.15	66.689
Area 6	BASE	100 Yr post	0.00	125.000	128.500	-0.0049	1162	24.097	0.00	209.038
Area 9	BASE	100 Yr post	12.15	127.063	129.500	0.0044	114	0.000	0.01	0.742
Area 1	BASE	100 Yr post	12.15	127.063	129.000	-0.0046	4366	31.406	12.54	35.572
Area 1	BASE	100 Yr post	12.30	124.554	128.500	0.0047	3800	95.612	12.15	99.101
Outfall	BASE	100 Yr post	30.00	120.000	121.000	0.0001	0	111.306	0.00	0.000
POND	BASE	100 Yr post	12.61	123.390	125.500	0.0029	174221	193.630	12.61	111.306
A	BASE	25 Yr post	12.07	125.847	129.000	-0.3000	3781	130.346	12.08	73.734
AA	BASE	25 Yr post	12.15	123.405	128.500	-0.0047	2430	52.679	12.17	52.769
Area 1B	BASE	25 Yr post	0.00	126.000	127.500	0.0041	7420	64.080	0.00	105.962
Area 1D	BASE	25 Yr post	12.12	124.187	128.500	-0.0047	3454	86.078	12.11	85.024
Area 3	BASE	25 Yr post	12.03	126.321	128.500	-0.0050	115	13.903	0.00	24.385
Area 4	BASE	25 Yr post	0.00	126.000	128.500	-0.0050	119	11.147	0.00	26.593
Area 5A	BASE	25 Yr post	0.00	129.000	133.000	-0.0049	2390	20.566	0.00	26.752
Area 5B	BASE	25 Yr post	12.09	125.834	129.000	0.0034	6239	29.268	12.00	40.437
Area 5C	BASE	25 Yr post	12.15	123.531	128.500	0.0035	7323	210.190	12.15	52.679
Area 6	BASE	25 Yr post	0.00	125.000	128.500	-0.0034	1162	19.098	0.00	209.038
Area 9	BASE	25 Yr post	0.00	127.000	129.500	-0.0050	114	0.000	0.01	0.742
Area 1	BASE	25 Yr post	0.00	127.000	129.000	-0.0050	4066	24.393	12.37	34.726
Area 1	BASE	25 Yr post	12.12	124.052	128.500	-0.0050	3467	85.024	12.14	85.273
Outfall	BASE	25 Yr post	30.00	120.000	121.000	0.0001	0	78.940	0.00	0.000
POND	BASE	25 Yr post	12.64	122.976	125.500	0.0026	171310	160.203	12.64	78.940

Appendix D

Stormwater Management Facility Operation & Maintenance Plan

Midulla Generating Station Stormwater Management Facility Operation and Maintenance Plan

This maintenance plan is for all stormwater management features constructed as part of the The stormwater management components consist of inlets, pipes, grassed ditches, and wet and dry stormwater ponds with control structures. The anticipated maintenance activities include de-silting of pipes and ponds, vegetation mowing and control, control structure cleaning, and erosion repair. The following requirements have been developed in anticipation of these maintenance and operation activities.

General Maintenance

1. All surface water management system pipes, inlets, catch basins, manholes, flumes, pond inflow and outfall structures (including oil skimmers), and discharge pipes should be inspected on a regular basis (monthly or quarterly) and after major rain-falls. They should be maintained by removing built-up debris and vegetation and repairing deteriorating structures.
2. Chemicals, oils, greases, cut or dead vegetation or similar wastes are NOT to be disposed of in the surface water management system or through storm sewers.
3. Accumulated pond sediments, stormwater swales, and culverts should be disposed of in an approved solid waste management facility.
4. During any repair or maintenance activity, use care to avoid causing erosion or siltation to adjacent or offsite areas. All retention/detention pond side slopes shall be sodded and staked as necessary, to prevent erosion.
5. Alterations (filling, enlarging, etc.) of any part of the surface water management system are not permitted without prior approval from the Department and all other applicable governing agencies.
6. Establishment and survival of littoral areas provided for stormwater quality treatment in wet detention system systems shall be assured by proper and continuing maintenance procedures designed to promote viable wetlands plant growth or natural diversity and character. Perpetual maintenance shall be provided for the certified system.

Inspections

1. The side slopes of the detention pond and adjoining swale shall be inspected for bare spots, damage or erosion. Bare areas shall be sodded or seeded to replace the grass cover. In the case of erosion, replace the missing soil and bring the affected areas back to grade.
2. On a quarterly basis and following significant storm events, inspect the area in front of the outfall control structure to for built-up sediments, vegetation and debris that

impair the operation of the structure. Remove sediments, vegetation, trash and debris to an approved disposal site.

3. When littoral zone vegetation and sediment accumulate to such an extent that water depth decreases, the littoral zone may need to be re-graded and re-vegetated. When it appears that the pond has reached this state, contact the Department prior to large scale maintenance.

Notify the Department at (813) 632-7600 within 24 hours of observation of sinkhole development in the surface water management system. All pipes will be de-silted once the accumulated sediment exceeds 25% of the available pipe cross-section for the full length of the pipe.

1. Accumulated sediment in the ponds shall be removed once the average depth of sediment over the entire pond area exceeds 6 inches as measured above the design pond bottom elevation. Upon removal of the sediment, the pond bottom shall be scarified with a disc harrow or similar device to facilitate percolation and recharge.
2. All pond control structures shall be inspected at least quarterly to insure proper operation of skimmers and discharge mechanisms. Accumulated debris shall be removed that would inhibit the proper operation of the control structure.

Erosion and sediment controls

The following discussion defines general guidelines for the sequence of construction and the use of stabilization and structural practices.

- Site Construction: Install silt fence on all sides draining off site. Install soil tracking prevention device at exit points to paved surfaces. Provide a temporary sedimentation basin, as necessary, during construction. Final grading will be done once the basin is permanently stabilized. Sod all disturbed areas after construction is completed.

The contractor will be required to review the site specific erosion control plan. The contractor may also be required to modify the plan or materials to adapt to seasonal variations or site conditions. Any modifications to this plan must be signed by a professional engineer representing the contractor. Contractor shall remove all sediment that has migrated off-site. The project engineer is responsible for determining if additional controls are needed and deployment schedules for the implementation of all erosion control devices.

Stabilization practices

Temporary:

- Seed and mulch, and sod.

All stabilization practices shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, but in no case more than 14 days after the construction activity in that portion of the site has temporarily or permanently ceased.

Structural Practices

All sediment controls shall be in place prior to any soil disturbing activity upstream of the control and may consist of one or more of the following.

- Silt Fence in accordance with FDOT Index 102.
- Sand bags.
- Hay bales.
- Berms.
- Timber bedding at construction areas.
- Turbidity barriers.
- Rip-Rap